

华中科技大学
Huazhong University of
Science and Technology

2009-2010学年度第一学期
2009.11.08—2010.01.30

《电力系统分析》 (I)

主讲教师：孙海顺

E-mail: haishunsun@hust.edu.cn

第七章 电力系统各元件的序阻抗和等值电路

7-1 对称分量法在不对称短路计算中的应用

7-2 同步发电机的负序和零序电抗

7-3 变压器的零序等值电路及其参数

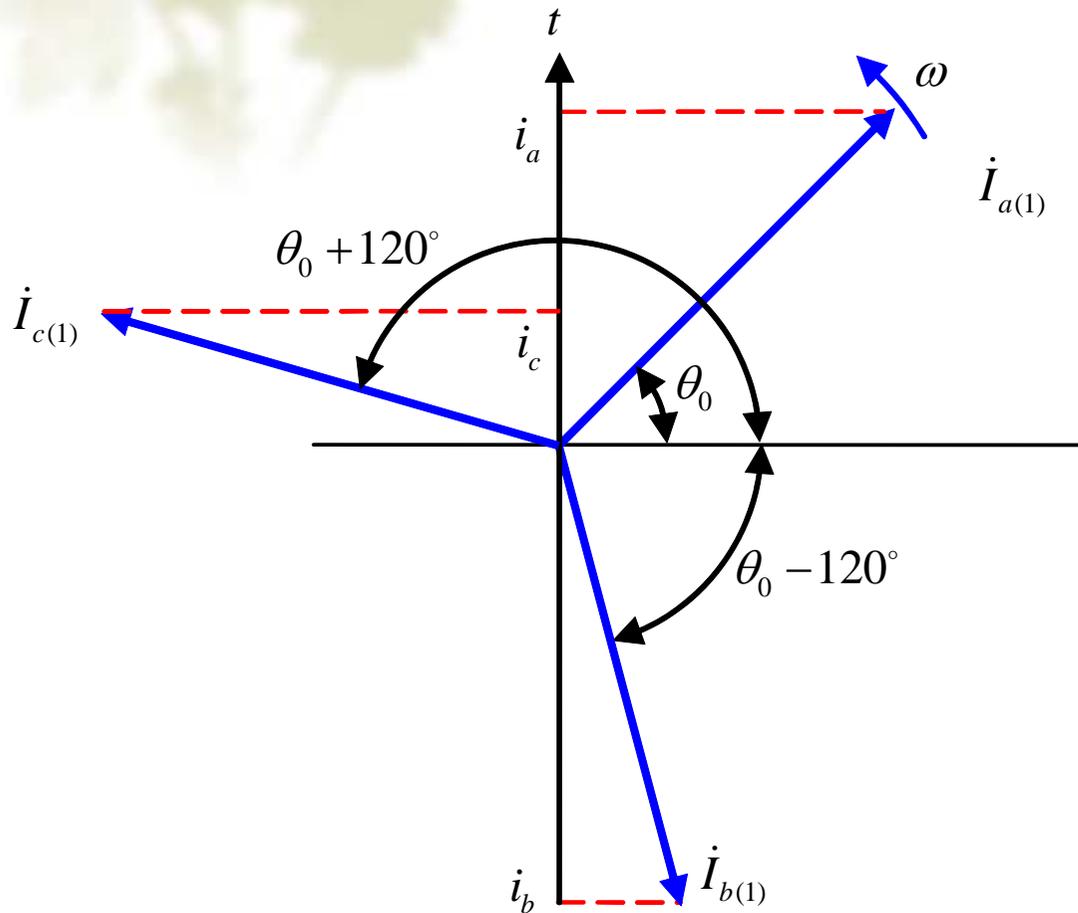
7-4 架空输电线路的零序阻抗及其等值电路

7-6 综合负荷的序阻抗

7-7 电力系统各序网络的制定

7-1 对称分量法在不对称短路计算中的应用

1. 不对称三相量的分解——对称分量



$$i_a = I_m \sin(\omega t + \theta_0)$$

$$i_b = I_m \sin(\omega t + \theta_0 - 120^\circ)$$

$$i_c = I_m \sin(\omega t + \theta_0 + 120^\circ)$$

正序分量:

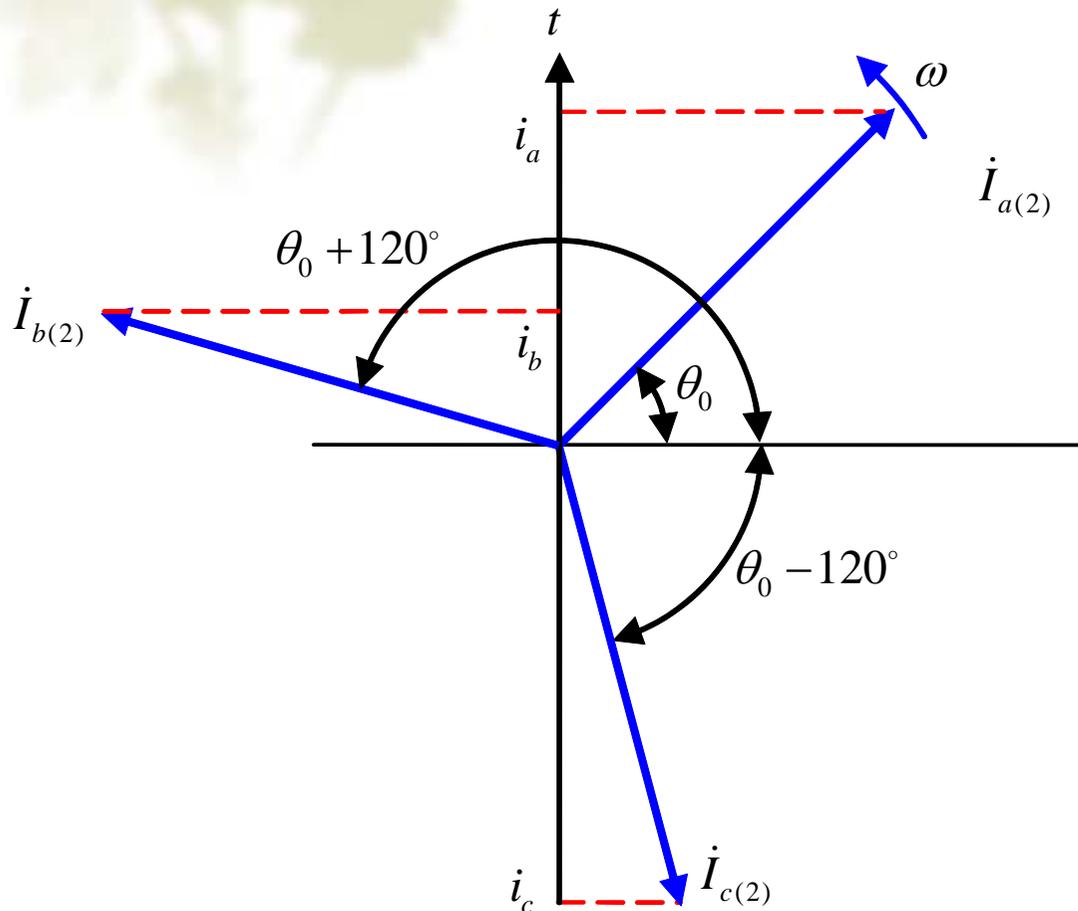
$$\dot{I}_{b(1)} = \alpha^2 \dot{I}_{a(1)} = e^{-j120^\circ} \dot{I}_{a(1)}$$

$$\dot{I}_{c(1)} = \alpha \dot{I}_{a(1)} = e^{j120^\circ} \dot{I}_{a(1)}$$

$$\alpha = e^{j120^\circ}, 1 + \alpha + \alpha^2 = 0$$

7-1 对称分量法在不对称短路计算中的应用

1. 不对称三相量的分解——对称分量



$$i_a = I_m \sin(\omega t + \theta_0)$$

$$i_b = I_m \sin(\omega t + \theta_0 + 120^\circ)$$

$$i_c = I_m \sin(\omega t + \theta_0 - 120^\circ)$$

负序分量:

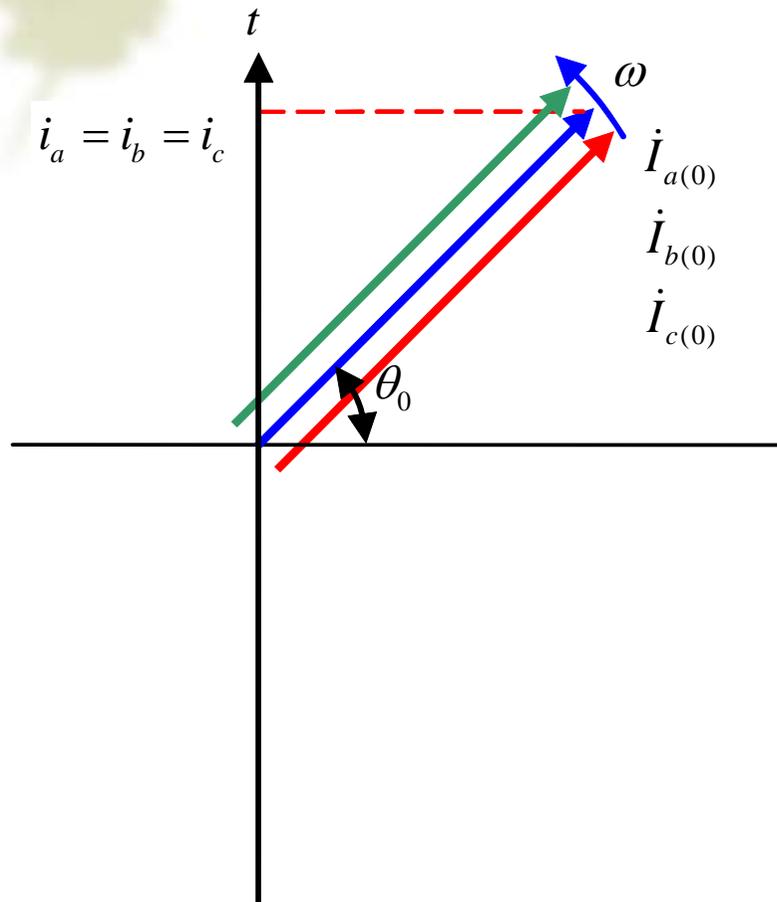
$$\dot{I}_{b(2)} = \alpha \dot{I}_{a(2)} = e^{j120^\circ} \dot{I}_{a(2)}$$

$$\dot{I}_{c(2)} = \alpha^2 \dot{I}_{a(2)} = e^{-j120^\circ} \dot{I}_{a(2)}$$

$$\alpha = e^{j120^\circ}, 1 + \alpha + \alpha^2 = 0$$

7-1 对称分量法在不对称短路计算中的应用

1. 不对称三相量的分解——对称分量



$$i_a = I_m \sin(\omega t + \theta_0)$$

$$i_b = I_m \sin(\omega t + \theta_0)$$

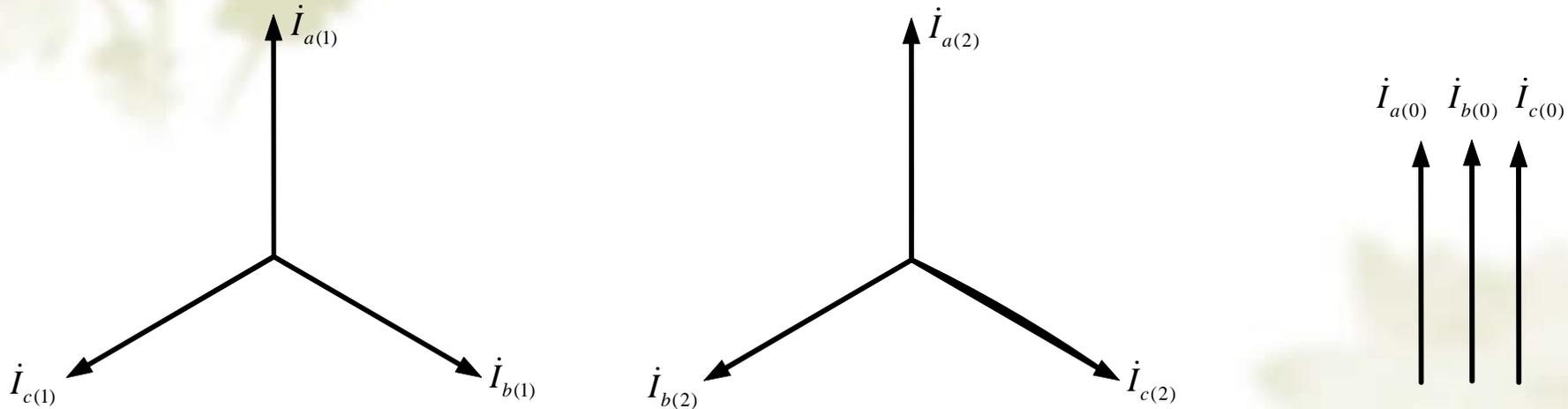
$$i_c = I_m \sin(\omega t + \theta_0)$$

零序分量:

$$\dot{I}_{a(0)} = \dot{I}_{b(0)} = \dot{I}_{c(0)}$$

7-1 对称分量法在不对称短路计算中的应用

1. 不对称三相量的分解——对称分量



正序分量:

$$\dot{I}_{b(1)} = \alpha^2 \dot{I}_{a(1)} = e^{-j120^\circ} \dot{I}_{a(1)}$$

$$\dot{I}_{c(1)} = \alpha \dot{I}_{a(1)} = e^{j120^\circ} \dot{I}_{a(1)}$$

负序分量:

$$\dot{I}_{b(2)} = \alpha \dot{I}_{a(2)} = e^{j120^\circ} \dot{I}_{a(2)}$$

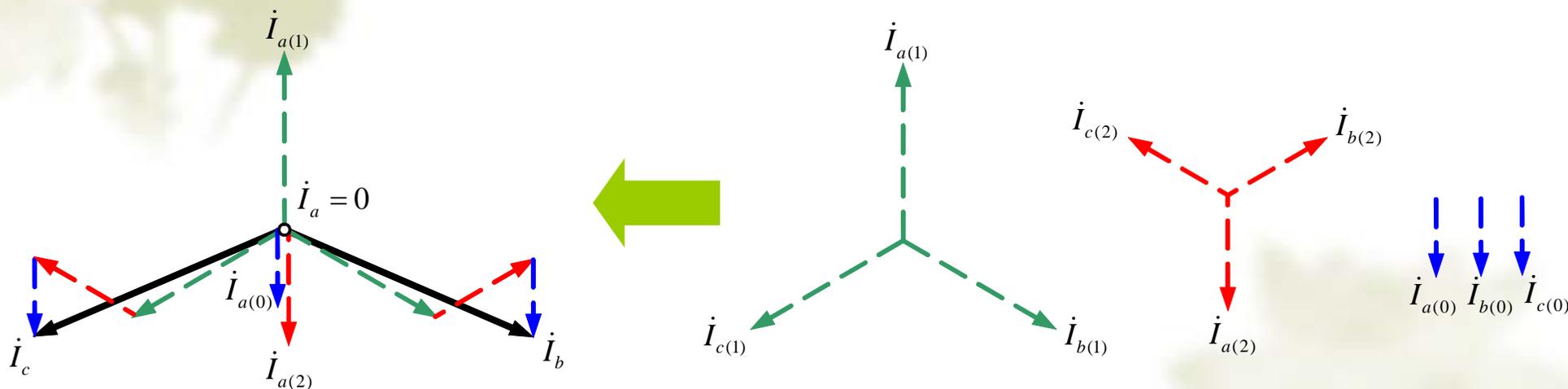
$$\dot{I}_{c(2)} = \alpha^2 \dot{I}_{a(2)} = e^{-j120^\circ} \dot{I}_{a(2)}$$

零序分量:

$$\dot{I}_{a(0)} = \dot{I}_{b(0)} = \dot{I}_{c(0)}$$

7-1 对称分量法在不对称短路计算中的应用

1. 不对称三相量的分解——对称分量分解



$$\begin{aligned} \dot{I}_a &= \dot{I}_{a(1)} + \dot{I}_{a(2)} + \dot{I}_{a(0)} \\ \dot{I}_b &= \dot{I}_{b(1)} + \dot{I}_{b(2)} + \dot{I}_{b(0)} \\ \dot{I}_c &= \dot{I}_{c(1)} + \dot{I}_{c(2)} + \dot{I}_{c(0)} \end{aligned}$$

以a相为基准相

$$\begin{aligned} \dot{I}_a &= \dot{I}_{a(1)} + \dot{I}_{a(2)} + \dot{I}_{a(0)} \\ \dot{I}_b &= \alpha^2 \dot{I}_{a(1)} + \alpha \dot{I}_{a(2)} + \dot{I}_{a(0)} \\ \dot{I}_c &= \alpha \dot{I}_{a(1)} + \alpha^2 \dot{I}_{a(2)} + \dot{I}_{a(0)} \end{aligned}$$

7-1 对称分量法在不对称短路计算中的应用

1. 不对称三相量的分解——对称分量分解

$$\begin{aligned} \dot{I}_a &= \dot{I}_{a(1)} + \dot{I}_{a(2)} + \dot{I}_{a(0)} \\ \dot{I}_b &= \alpha^2 \dot{I}_{a(1)} + \alpha \dot{I}_{a(2)} + \dot{I}_{a(0)} \\ \dot{I}_c &= \alpha \dot{I}_{a(1)} + \alpha^2 \dot{I}_{a(2)} + \dot{I}_{a(0)} \end{aligned}$$

$$\begin{bmatrix} \dot{I}_a \\ \dot{I}_b \\ \dot{I}_c \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 \\ \alpha^2 & \alpha & 1 \\ \alpha & \alpha^2 & 1 \end{bmatrix} \begin{bmatrix} \dot{I}_{a(1)} \\ \dot{I}_{a(2)} \\ \dot{I}_{a(0)} \end{bmatrix}$$

$$\dot{\mathbf{I}}_{120} = \mathbf{S} \dot{\mathbf{I}}_{abc}$$

$$\dot{\mathbf{I}}_{abc} = \mathbf{S}^{-1} \dot{\mathbf{I}}_{120}$$

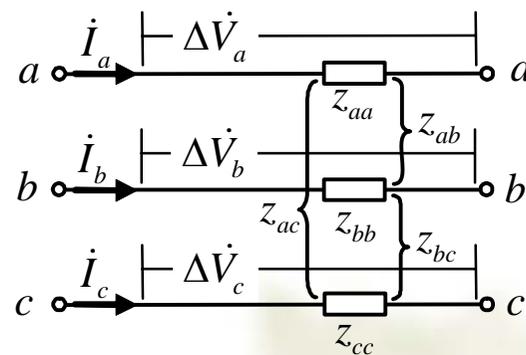
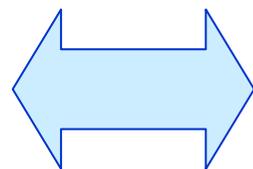
$$\begin{bmatrix} \dot{I}_{a(1)} \\ \dot{I}_{a(2)} \\ \dot{I}_{a(0)} \end{bmatrix} = \frac{1}{3} \begin{bmatrix} 1 & \alpha & \alpha^2 \\ 1 & \alpha^2 & \alpha \\ 1 & 1 & 1 \end{bmatrix} \begin{bmatrix} \dot{I}_a \\ \dot{I}_b \\ \dot{I}_c \end{bmatrix}$$

$$\dot{\mathbf{I}}_{abc} \xleftrightarrow{\text{唯一变换}} \dot{\mathbf{I}}_{120}$$

7-1 对称分量法在不对称短路计算中的应用

2. 序阻抗的概念——三相对称电路

$$\begin{bmatrix} \Delta \dot{V}_a \\ \Delta \dot{V}_b \\ \Delta \dot{V}_c \end{bmatrix} = \begin{bmatrix} Z_{aa} & Z_{ab} & Z_{ca} \\ Z_{ab} & Z_{bb} & Z_{bc} \\ Z_{ca} & Z_{bc} & Z_{cc} \end{bmatrix} \begin{bmatrix} \dot{I}_a \\ \dot{I}_b \\ \dot{I}_c \end{bmatrix}$$



$$\Delta \dot{\mathbf{V}}_{abc} = \mathbf{Z} \dot{\mathbf{I}}_{abc}$$

$$\Delta \dot{\mathbf{V}}_{120} = \mathbf{S} \Delta \dot{\mathbf{V}}_{abc} = \mathbf{S} \mathbf{Z} \mathbf{S}^{-1} \mathbf{S} \dot{\mathbf{I}}_{abc} = \mathbf{Z}_{SC} \dot{\mathbf{I}}_{120}$$

$$\begin{bmatrix} \Delta \dot{V}_{a(1)} \\ \Delta \dot{V}_{a(2)} \\ \Delta \dot{V}_{a(0)} \end{bmatrix} = \begin{bmatrix} Z_s - Z_m & 0 & 0 \\ 0 & Z_s - Z_m & 0 \\ 0 & 0 & Z_s + 2Z_m \end{bmatrix} \begin{bmatrix} \dot{I}_{a(1)} \\ \dot{I}_{a(2)} \\ \dot{I}_{a(0)} \end{bmatrix}$$



三相对称电路

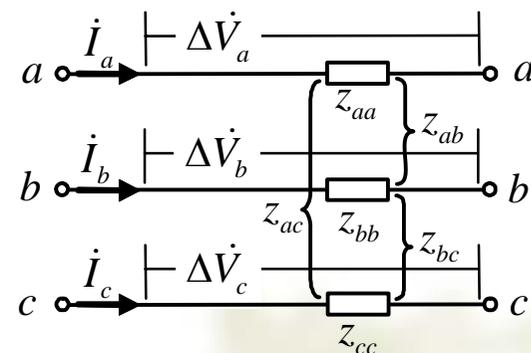
$$Z_{aa} = Z_{bb} = Z_{cc} = Z_s$$

$$Z_{ab} = Z_{bc} = Z_{ca} = Z_m$$

7-1 对称分量法在不对称短路计算中的应用

2. 序阻抗的概念—定义

$$\begin{bmatrix} \Delta \dot{V}_{a(1)} \\ \Delta \dot{V}_{a(2)} \\ \Delta \dot{V}_{a(0)} \end{bmatrix} = \begin{bmatrix} z_s - z_m & 0 & 0 \\ 0 & z_s - z_m & 0 \\ 0 & 0 & z_s + 2z_m \end{bmatrix} \begin{bmatrix} \dot{I}_{a(1)} \\ \dot{I}_{a(2)} \\ \dot{I}_{a(0)} \end{bmatrix}$$



$$\Delta \dot{V}_{a(1)} = (z_s - z_m) \dot{I}_{a(1)}$$

$$\Delta \dot{V}_{b(1)} = (z_s - z_m) \dot{I}_{b(1)}$$

$$\Delta \dot{V}_{c(1)} = (z_s - z_m) \dot{I}_{c(1)}$$

$$\Delta \dot{V}_{a(2)} = (z_s - z_m) \dot{I}_{a(2)}$$

$$\Delta \dot{V}_{b(2)} = (z_s - z_m) \dot{I}_{b(2)}$$

$$\Delta \dot{V}_{c(2)} = (z_s - z_m) \dot{I}_{c(2)}$$

$$\Delta \dot{V}_{a(0)} = (z_s + 2z_m) \dot{I}_{a(0)}$$

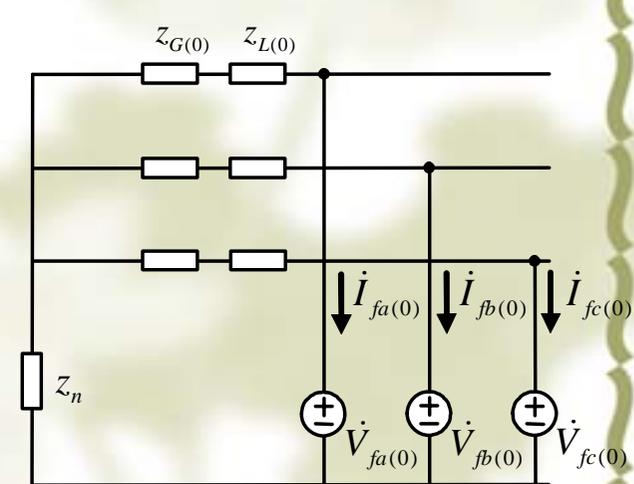
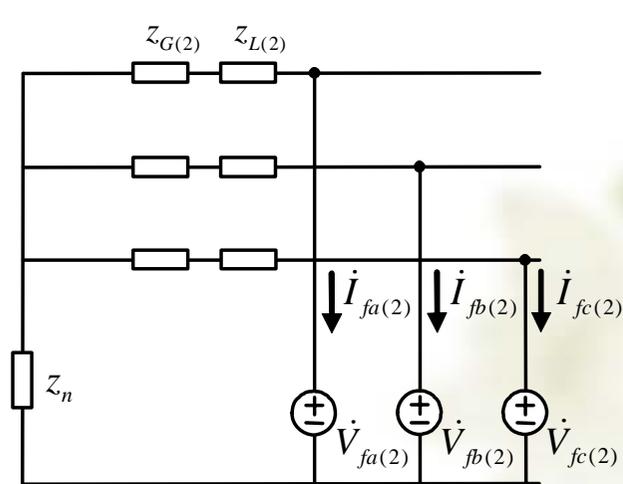
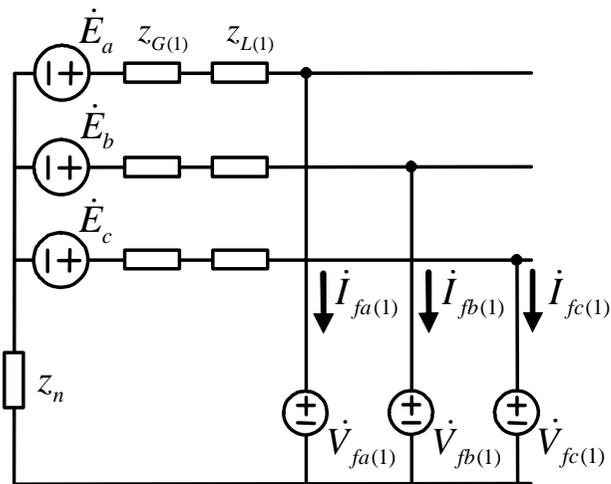
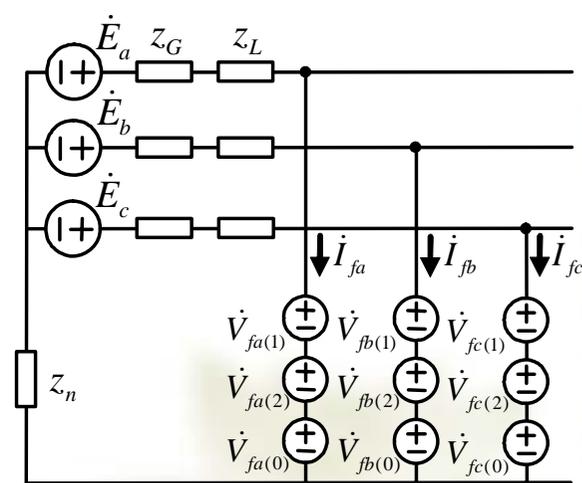
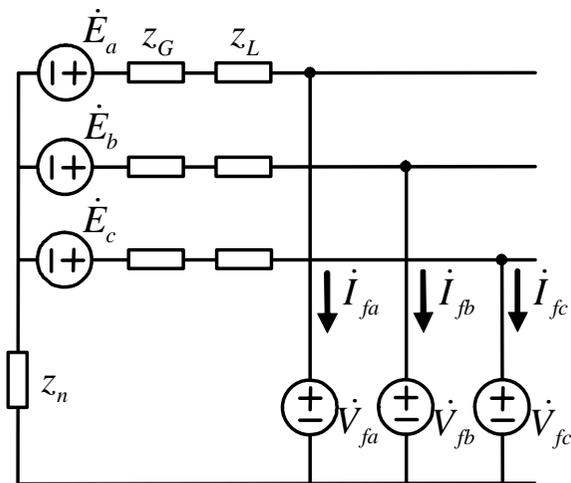
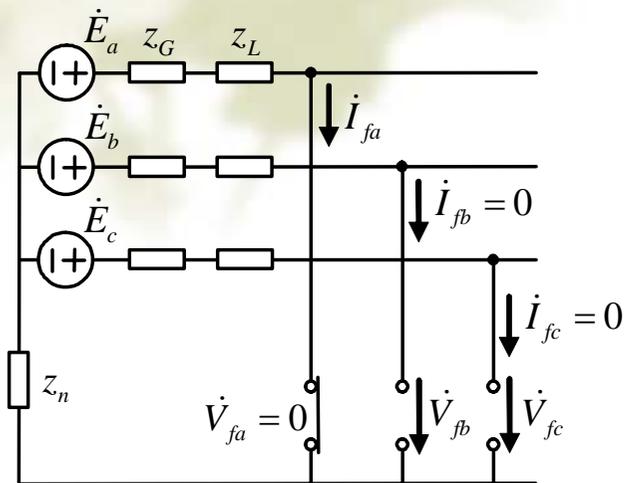
$$\Delta \dot{V}_{b(0)} = (z_s + 2z_m) \dot{I}_{b(0)}$$

$$\Delta \dot{V}_{c(0)} = (z_s + 2z_m) \dot{I}_{c(0)}$$

序阻抗定义: $z_{(1)} = \Delta \dot{V}_{a(1)} / \dot{I}_{a(1)}$, $z_{(2)} = \Delta \dot{V}_{a(2)} / \dot{I}_{a(2)}$, $z_{(0)} = \Delta \dot{V}_{a(0)} / \dot{I}_{a(0)}$

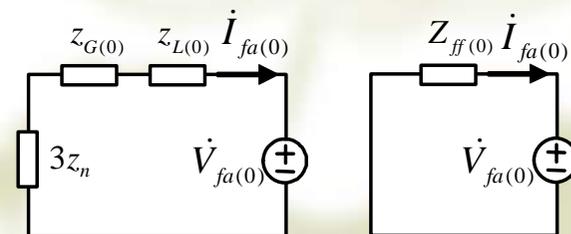
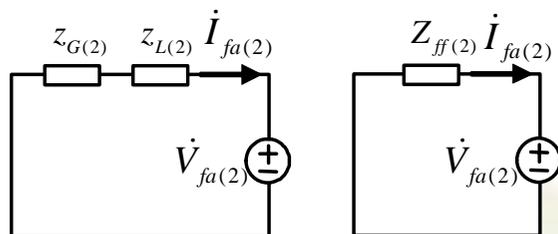
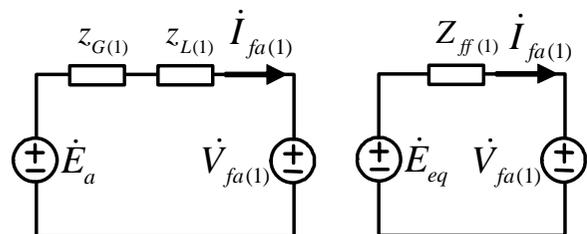
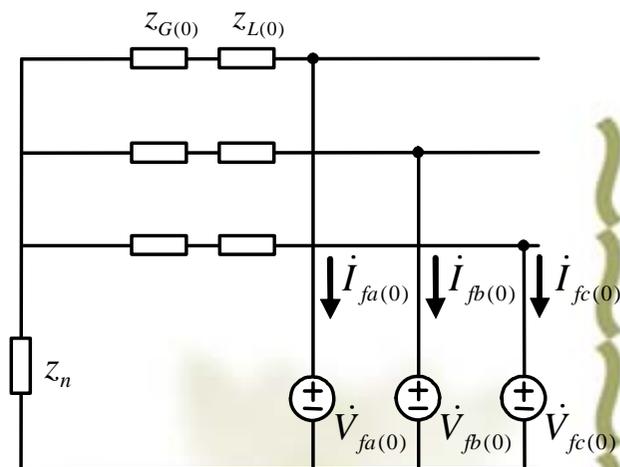
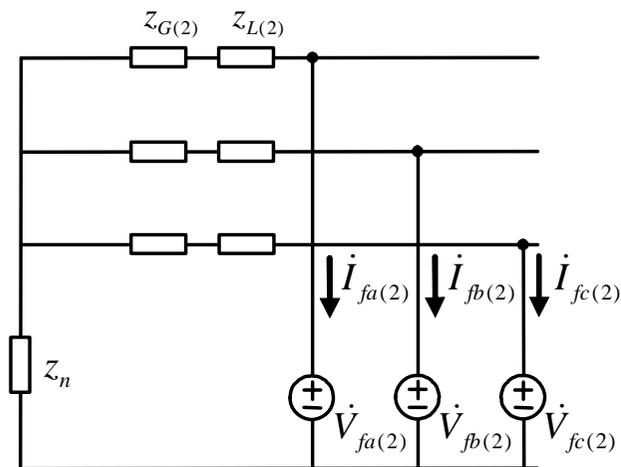
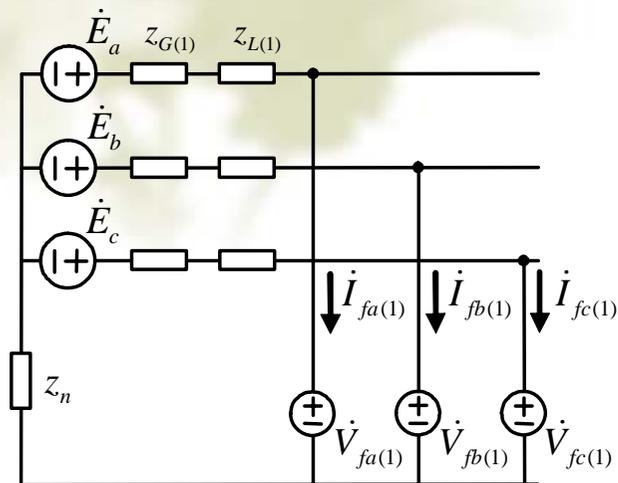
7-1 对称分量法在不对称短路计算中的应用

3. 对称分量法在不对称短路计算中的应用



7-1 对称分量法在不对称短路计算中的应用

3. 对称分量法在不对称短路计算中的应用



$$\dot{V}_{fa(1)} = \dot{E}_{eq} - Z_{ff(1)} \dot{I}_{fa(1)}$$

$$\dot{V}_{fa(2)} = -Z_{ff(2)} \dot{I}_{fa(2)}$$

$$\dot{V}_{fa(0)} = -Z_{ff(0)} \dot{I}_{fa(0)}$$

7-1 对称分量法在不对称短路计算中的应用

3. 对称分量法在不对称短路计算中的应用

基本方法：用一组不对称电势源代替故障口的结构不对称

然后对称分量分解

基本前提：

三相对称——各序分量

独立；

线性网络——叠加原

理；

序网方程

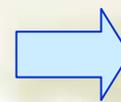
$$\dot{V}_{fa(1)} = \dot{E}_{eq} - Z_{ff(1)} \dot{I}_{fa(1)}$$

$$\dot{V}_{fa(2)} = -Z_{ff(2)} \dot{I}_{fa(2)}$$

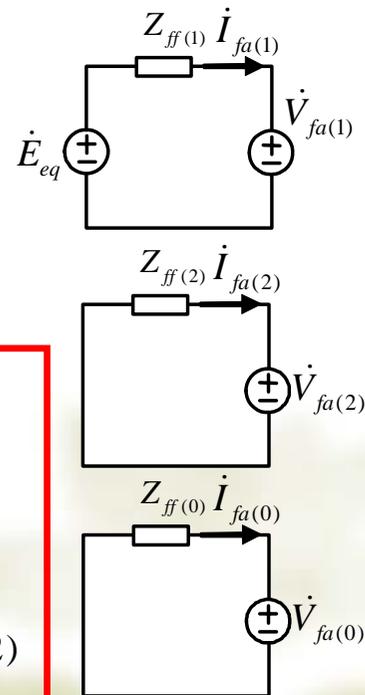
$$\dot{V}_{fa(0)} = -Z_{ff(0)} \dot{I}_{fa(0)}$$

+

故障口边界条件



Solution



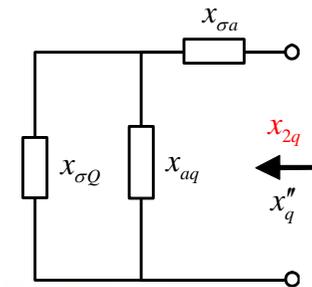
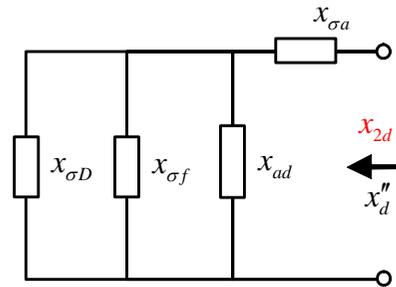
7-2 同步电机的负序和零序电抗

1. 确定发电机负序电抗的等值电路和计算公式

$$f^{(1)}: x_{(2)}^{(1)} = \sqrt{\left(x_d'' + \frac{x_{(0)}}{2}\right)\left(x_q'' + \frac{x_{(0)}}{2}\right)} - \frac{x_{(0)}}{2}$$

$$f^{(2)}: x_{(2)}^{(2)} = \sqrt{x_d'' x_q''}$$

$$f^{(1,1)}: x_{(2)}^{(1,1)} = \frac{x_d'' x_q'' + \sqrt{x_d'' x_q'' (2x_{(0)} + x_d'')(2x_{(0)} + x_q'')}}{2x_{(0)} + x_d'' + x_q''}$$



$$x_{(2)} = \frac{1}{2}(x_d'' + x_q'')$$

$$x_{(2)} = \sqrt{x_d' x_q''}$$

表7-2 同步电机负序和零序电抗的典型值

电机类型	$x_{(2)}$	$x_{(0)}$	电机类型	$x_{(2)}$	$x_{(0)}$
汽轮发电机	0.16	0.06	无阻尼绕组水轮发电机	0.45	0.07
有阻尼绕组水轮发电机	0.25	0.07	同步调相机、大型同步电动机	0.24	0.08

7-3 变压器的零序等值电路及其参数

1. 普通变压器的零序等值电路

$$F_1 = w_1 \dot{I}_1, \quad \dot{\phi}_{1\sigma} = F_1 \Lambda_{1\sigma} = w_1 \Lambda_{1\sigma} \dot{I}_1$$

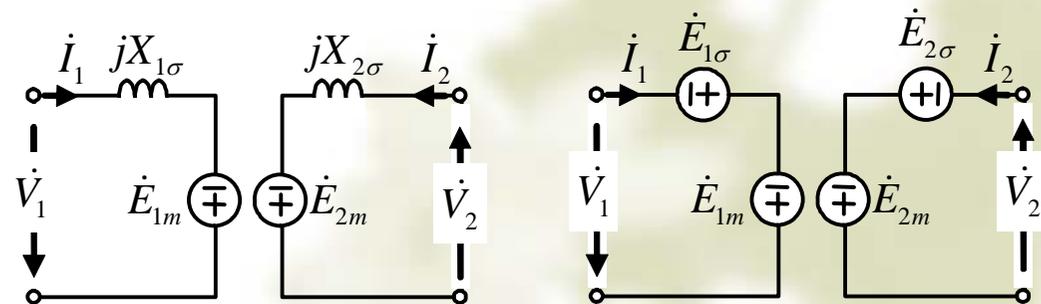
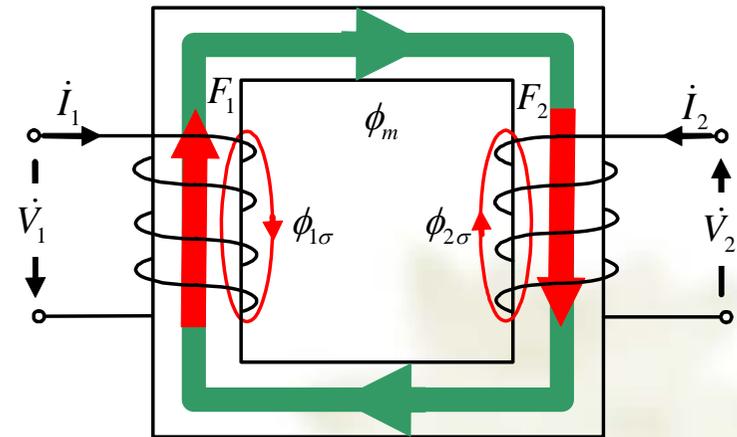
$$\dot{E}_{1\sigma} = -j\omega w_1 \dot{\phi}_{1\sigma} = -j\omega w_1^2 \Lambda_{1\sigma} \dot{I}_1$$

$$-\dot{E}_{1\sigma} = jX_{1\sigma} \dot{I}_1, \quad X_{1\sigma} = \omega w_1^2 \Lambda_{1\sigma}$$

$$\text{同理有: } -\dot{E}_{2\sigma} = jX_{2\sigma} \dot{I}_2$$

$$\begin{aligned} \dot{V}_1 &= -\dot{E}_{1\sigma} - \dot{E}_{1m} \\ &= jX_{1\sigma} \dot{I}_1 - \dot{E}_{1m} \end{aligned}$$

$$\dot{V}_2 = \dot{E}_{2\sigma} + \dot{E}_{2m}$$



7-3 变压器的零序等值电路及其参数

1. 普通变压器的零序等值电路

$$\begin{aligned}\dot{\phi}_m &= (F_1 + F_2) \Lambda_m = (w_1 \dot{I}_1 + w_2 \dot{I}_2) \Lambda_m \\ &= w_1 (\dot{I}_1 + \dot{I}'_2) \Lambda_m = w_1 \dot{I}_m \Lambda_m\end{aligned}$$

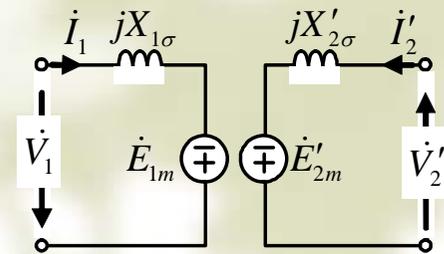
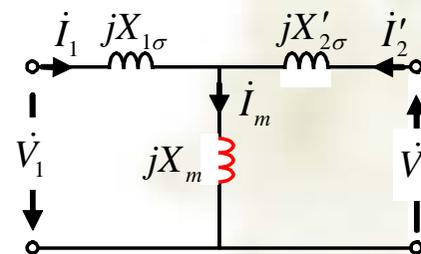
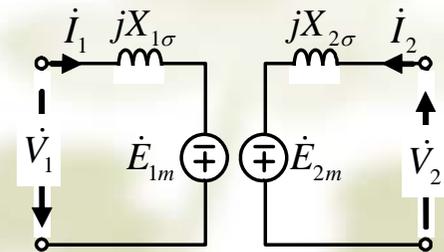
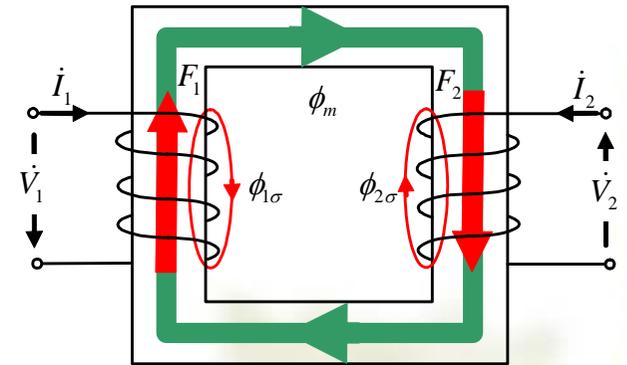
$$\dot{E}_{1m} = -j\omega w_1 \dot{\phi}_m = -j\omega w_1^2 \Lambda_m \dot{I}_m$$

$$\dot{E}_{2m} = -j\omega w_2 \dot{\phi}_m = -j\omega w_2 w_1 \Lambda_m \dot{I}_m$$

$$\dot{E}'_{2m} = (w_1/w_2) \dot{E}_{2m} = -j\omega w_1^2 \Lambda_m \dot{I}_m$$

$$-\dot{E}_{1m} = jX_m \dot{I}_m = jX_m (\dot{I}_1 + \dot{I}'_2)$$

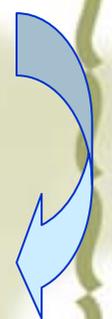
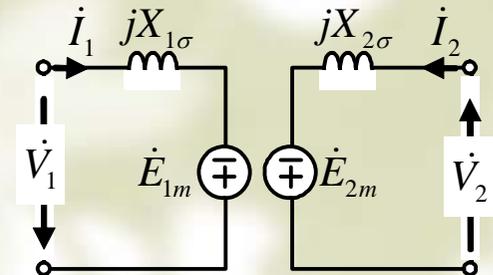
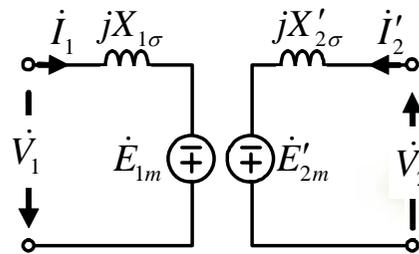
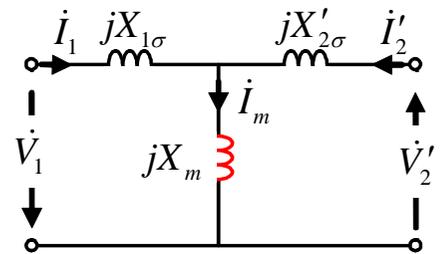
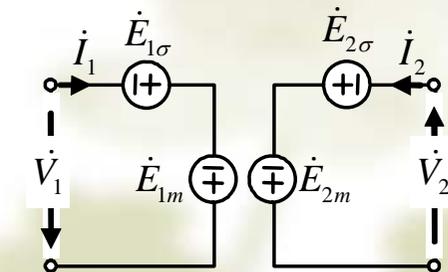
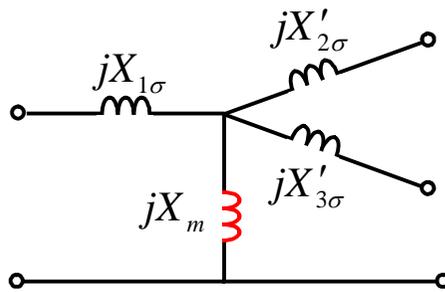
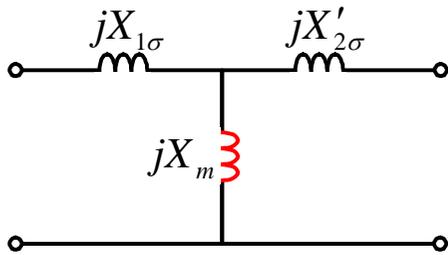
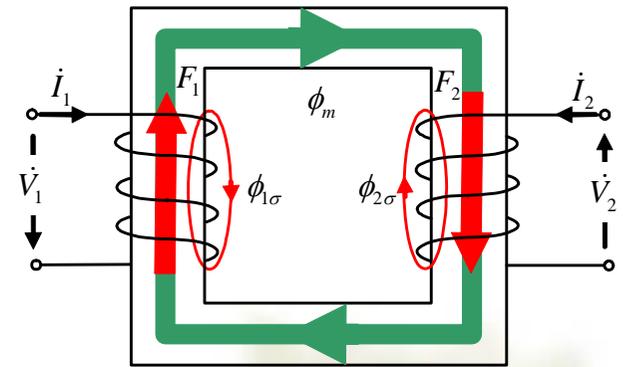
$$-\dot{E}'_{2m} = jX_m \dot{I}_m = jX_m (\dot{I}_1 + \dot{I}'_2)$$



7-3 变压器的零序等值电路及其参数

1. 普通变压器的零序等值电路——结论1

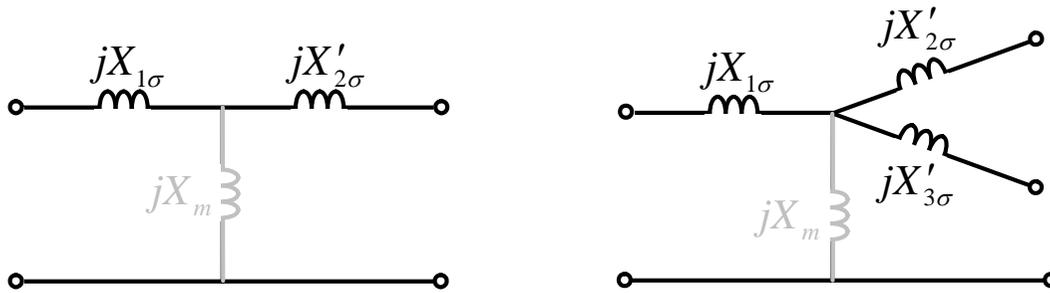
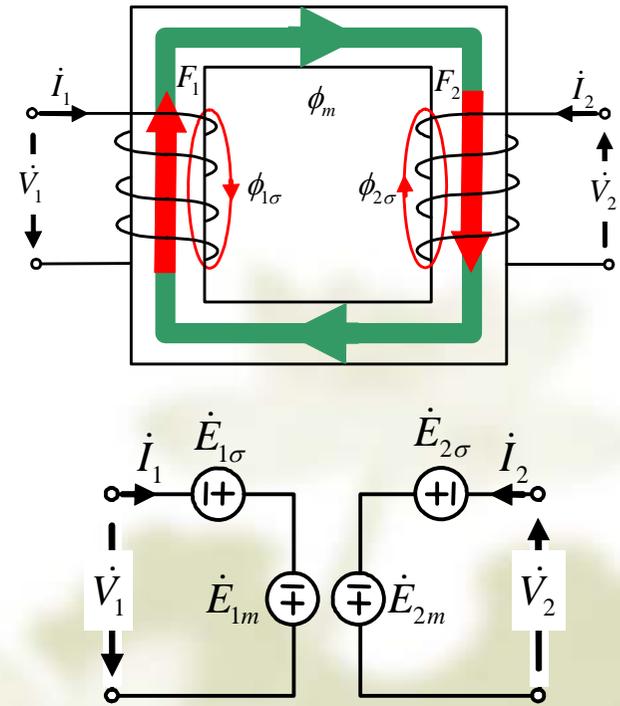
(1) **电路结构相同**——变压器的一相等值电路反应了原副方的电磁耦合关系，对各序电流这种耦合关系相同；



7-3 变压器的零序等值电路及其参数

1. 普通变压器的零序等值电路——结论2

(2) 各序漏电抗相等——等值电路中采用漏电抗压降表示漏磁通感生的电势，漏电抗数值取决于对应的漏磁通路径的磁导率，绕组通过各序电流，其漏磁通路径相同，并且磁导率为常数 $X_{\sigma(1)} = X_{\sigma(2)} = X_{\sigma(0)}$;

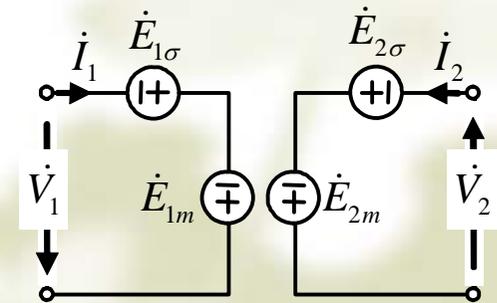
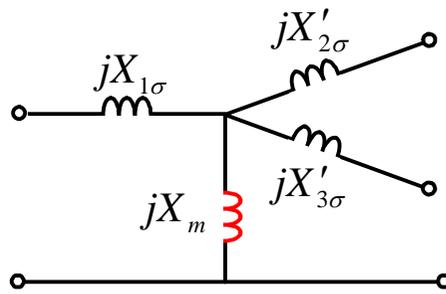
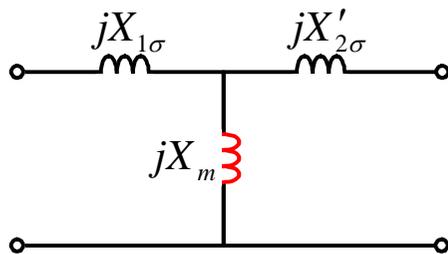
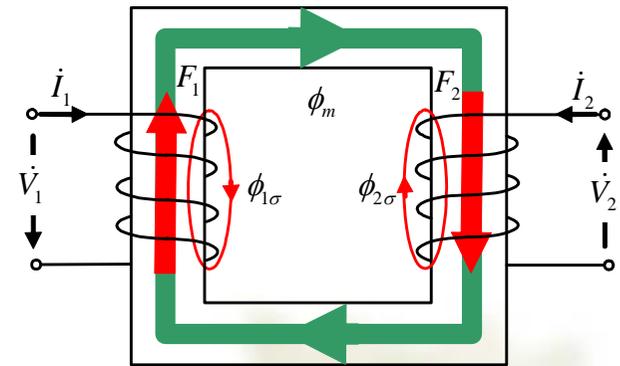


$$-\dot{E}_{1\sigma} = jX_{1\sigma} \dot{I}_1, \quad X_{1\sigma} = \omega w_1^2 \Lambda_{1\sigma}, \quad -\dot{E}_{2\sigma} = jX_{2\sigma} \dot{I}_2, \quad X_{2\sigma} = \omega w_2^2 \Lambda_{1\sigma},$$

7-3 变压器的零序等值电路及其参数

1. 普通变压器的零序等值电路——结论3

(3) 零序激磁电抗与变压器铁芯结构相关——变压器主磁通感生的电势用激磁电抗压降表示，激磁电抗数值取决于主磁通路径的磁导率；

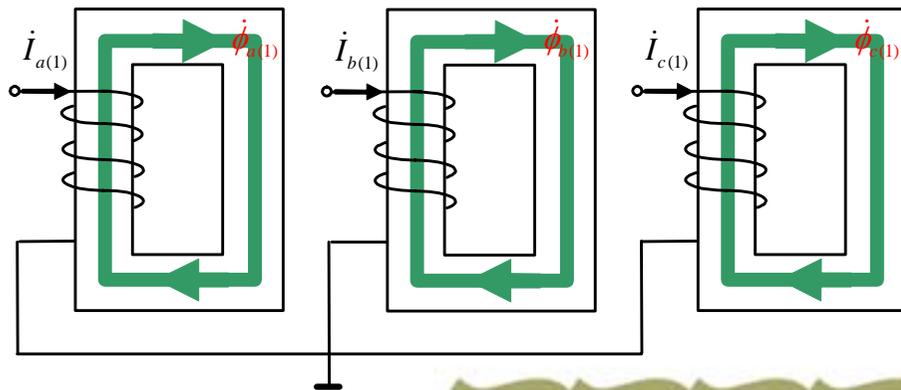
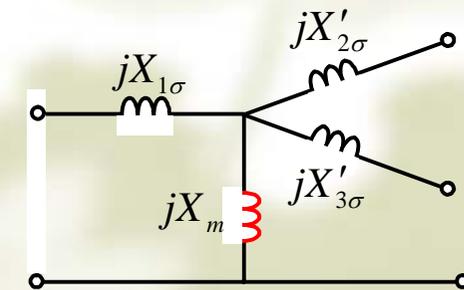
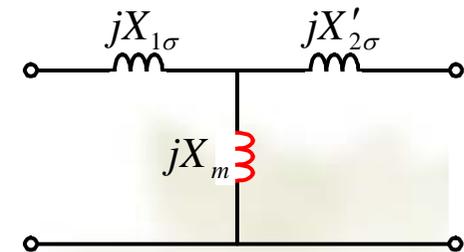
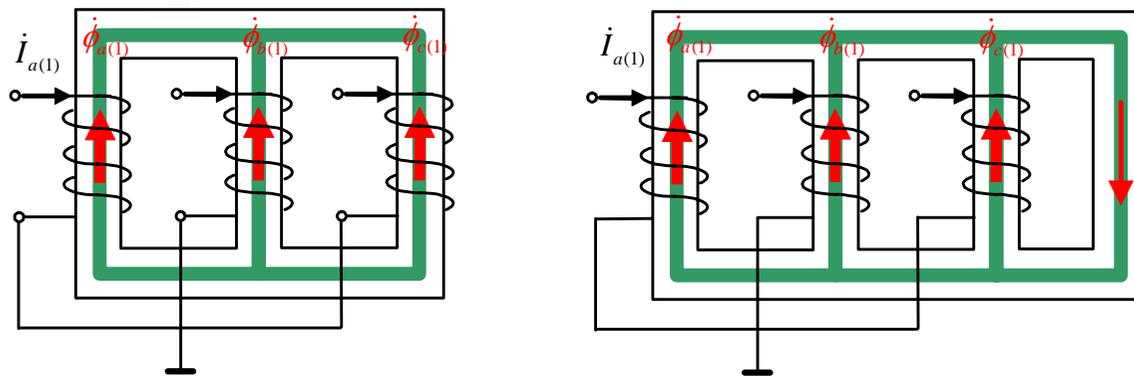


$$-\dot{E}_{1m} = j\omega w_1^2 \Lambda_m \dot{I}_m = jX_m \dot{I}_m, \quad -\dot{E}'_{2m} = j\omega w_2^2 \Lambda_m \dot{I}_m = jX_m \dot{I}_m$$

7-3 变压器的零序等值电路及其参数

1. 普通变压器的零序等值电路——结论4

(4) 绕组通过正序或者负序电流，主磁通路径都是铁芯， $X_{m(1)} = X_{m(2)}$ ，并且磁导率远大于漏磁通路径，因此 $X_{m(1)}$ 远大于 $X_{\sigma(1)}$ ；



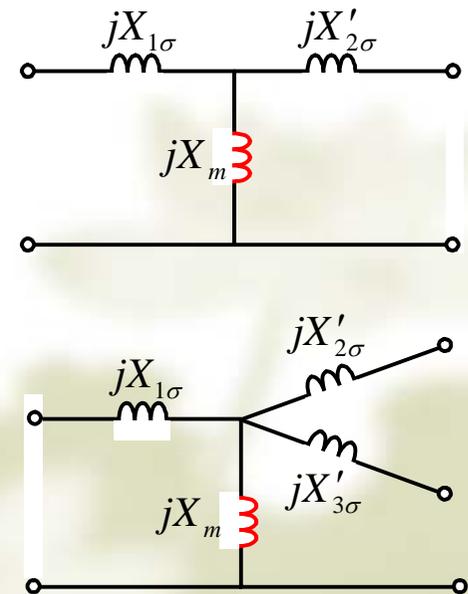
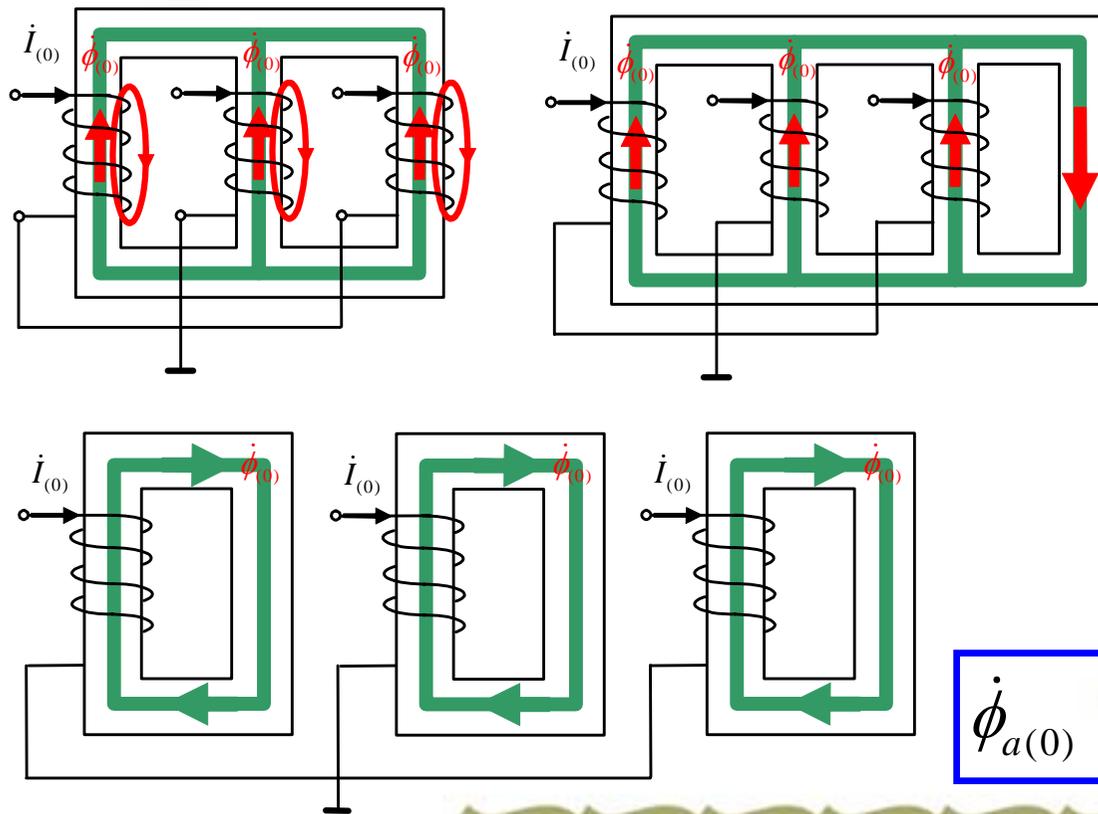
$$\dot{\phi}_{a(1)} + \dot{\phi}_{b(1)} + \dot{\phi}_{c(1)} = 0$$

$$X_m = \omega w_1^2 \Lambda_m$$

7-3 变压器的零序等值电路及其参数

1. 普通变压器的零序等值电路——结论5

(5) 绕组通过零序电流，三相三柱式变压器零序主磁通路径只能沿铁芯和空气构成回路，磁导率与漏磁通路径相当，因此 $X_{m(0)} < X_{m(1)}$ ；其他铁芯结构， $X_{m(0)} = X_{m(1)}$ ；

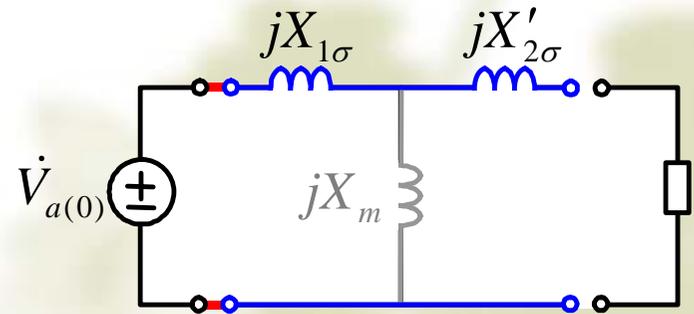
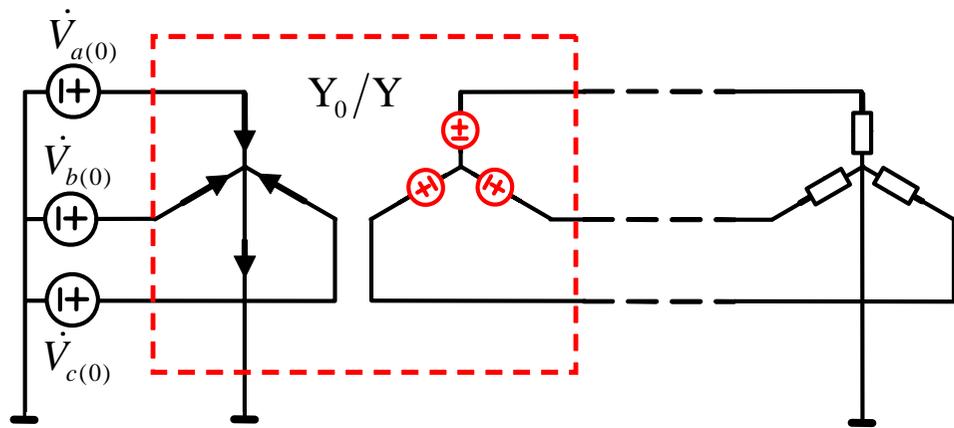
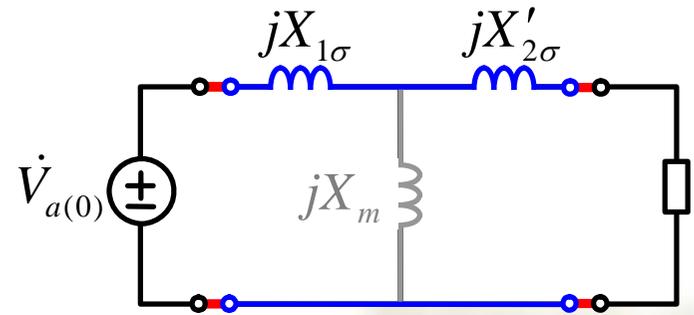
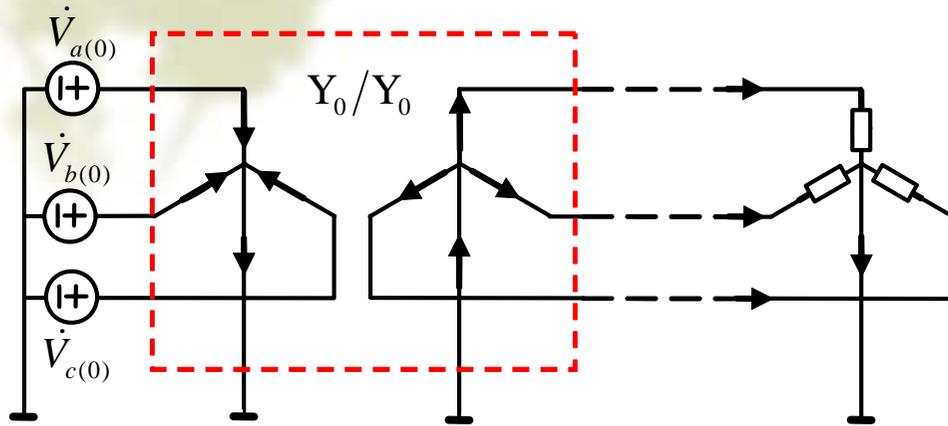


$$\dot{\phi}_{a(0)} = \dot{\phi}_{b(0)} = \dot{\phi}_{c(0)}$$

$$X_m = \omega w_1^2 \Lambda_m$$

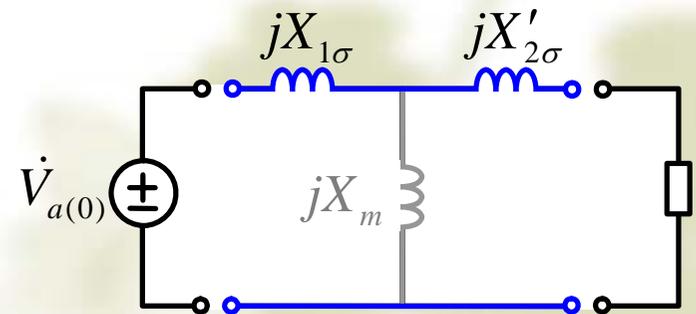
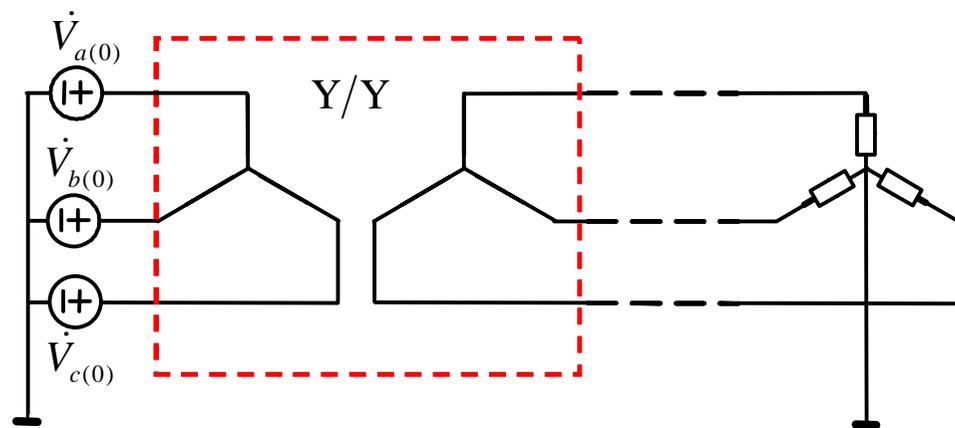
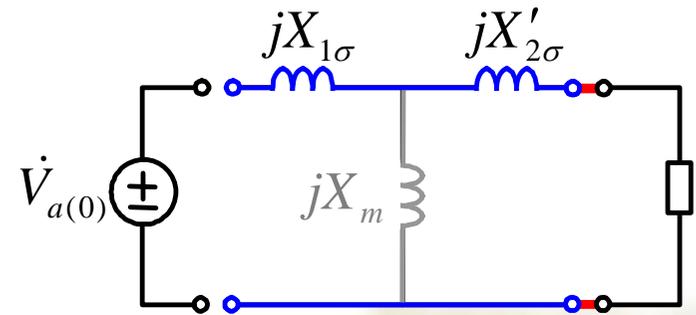
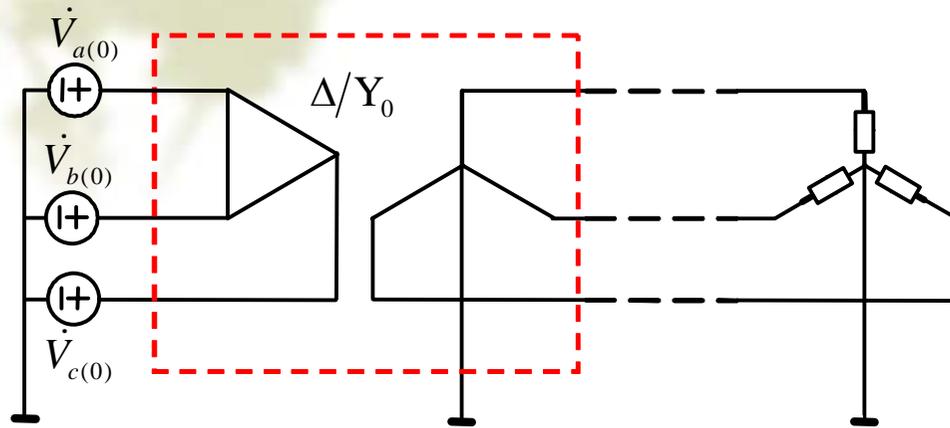
7-3 变压器的零序等值电路及其参数

2. 变压器的零序等值电路与外电路的联接



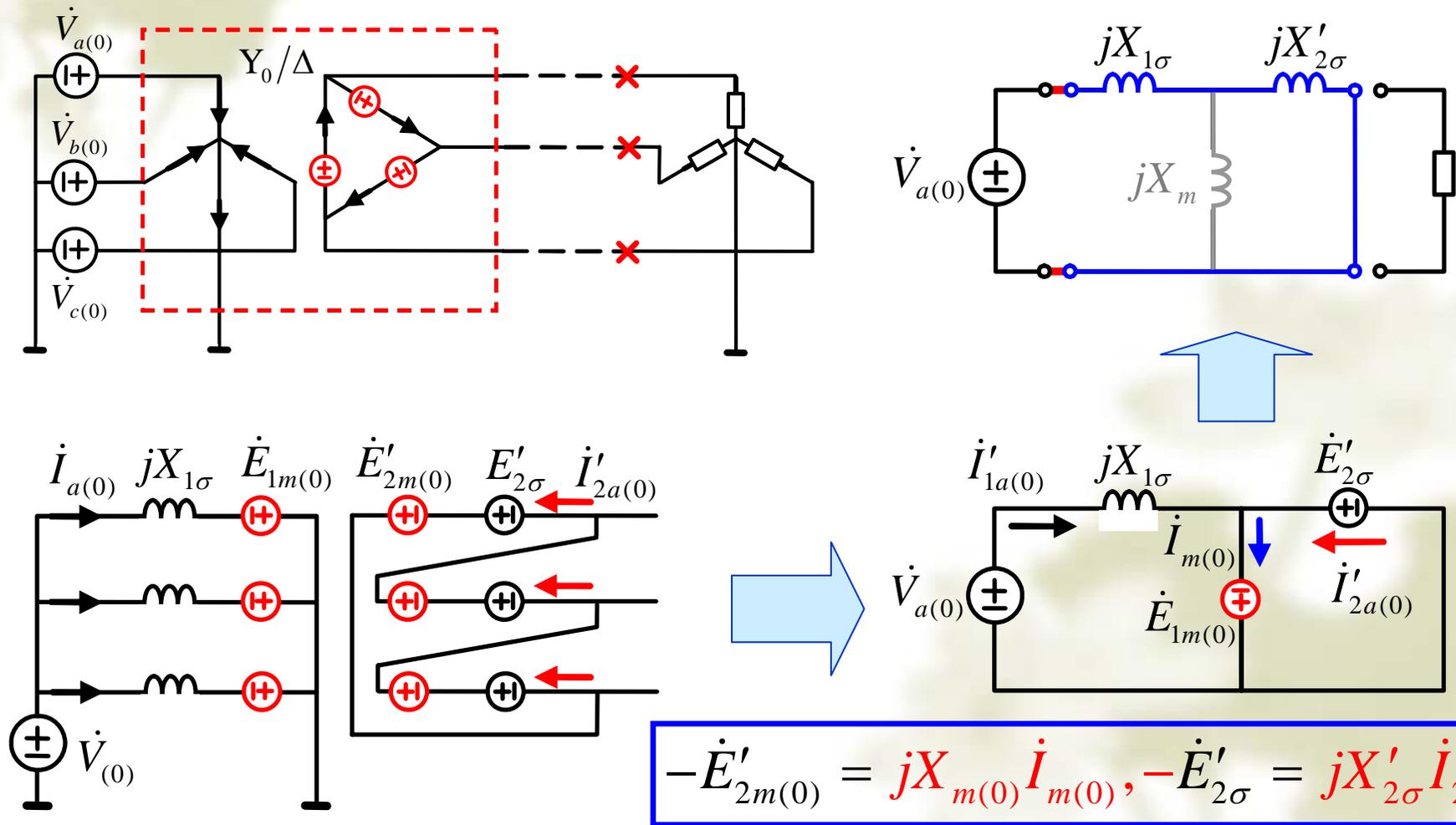
7-3 变压器的零序等值电路及其参数

2. 变压器的零序等值电路与外电路的联接

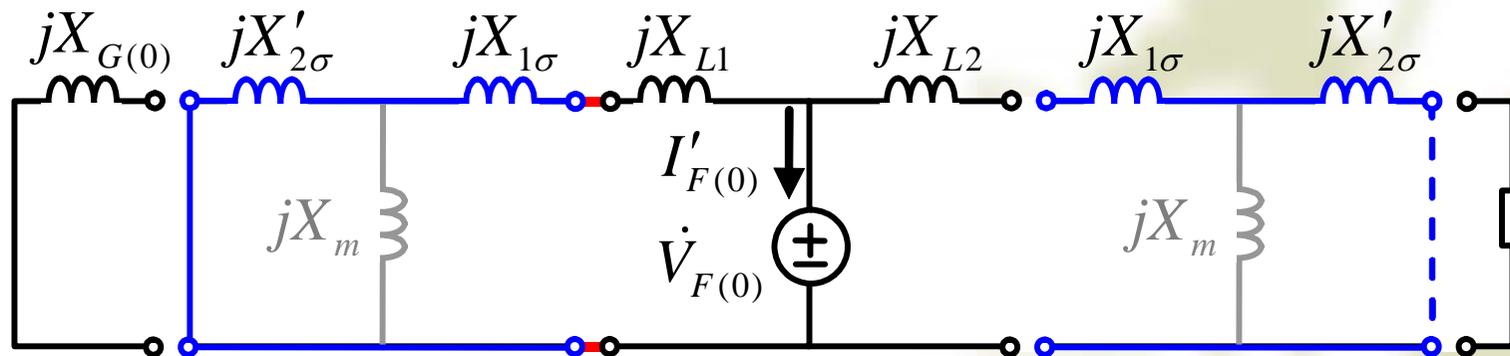
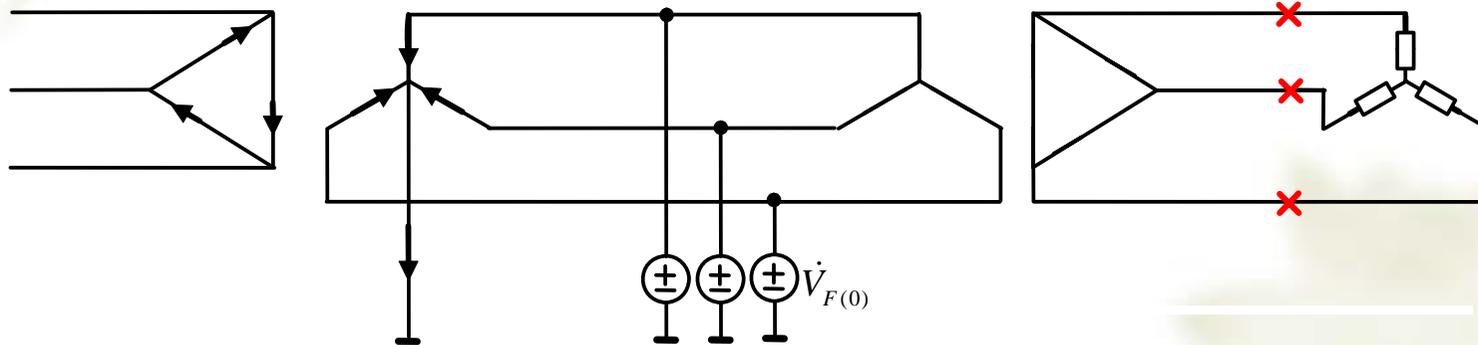
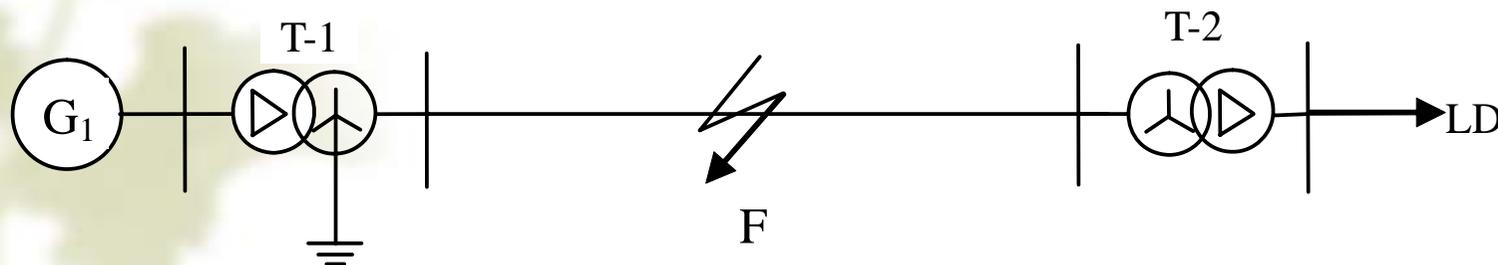


7-3 变压器的零序等值电路及其参数

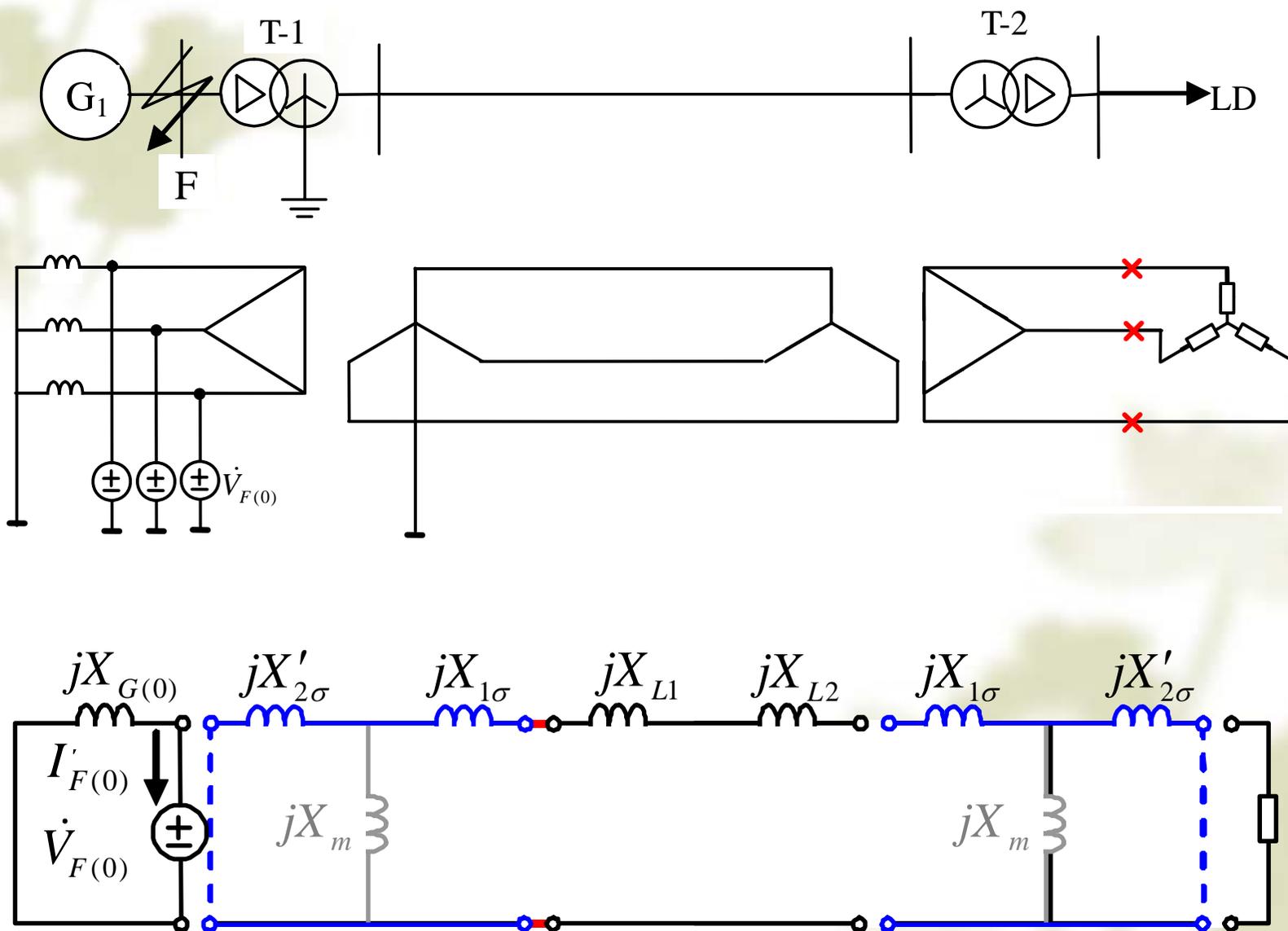
2. 变压器的零序等值电路与外电路的联接



2. 变压器的零序等值电路与外电路的联接——举例

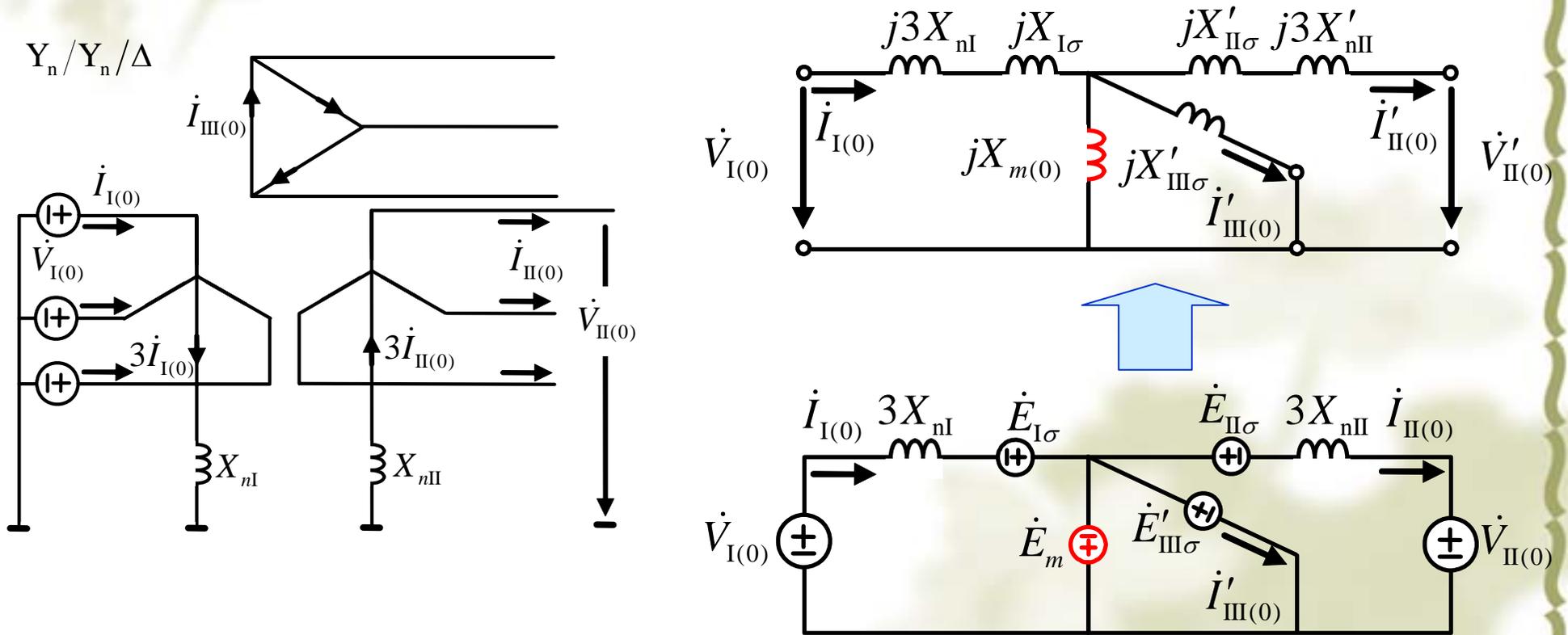


2. 变压器的零序等值电路与外电路的联接——举例



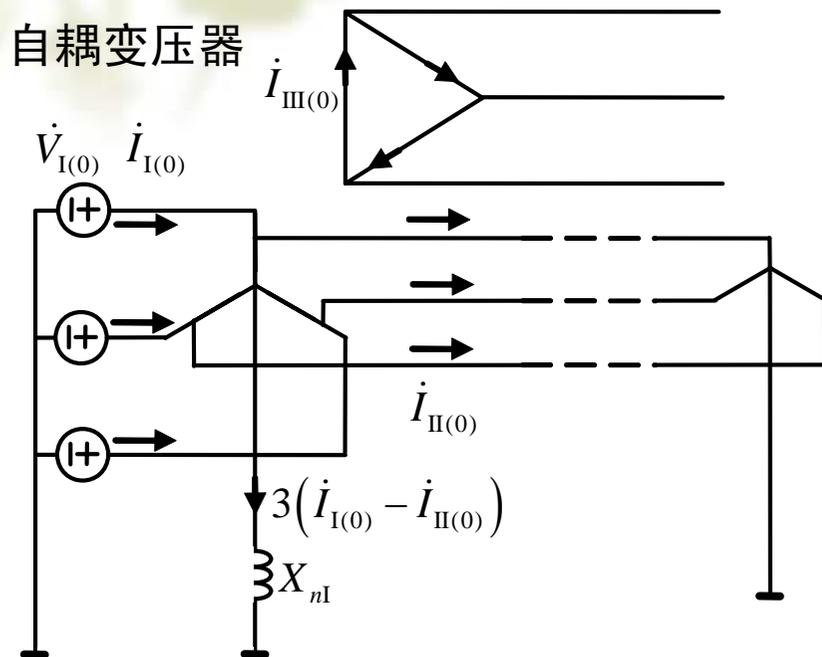
7-3 变压器的零序等值电路及其参数

3. 中性点有接地阻抗的变压器零序等值电路



7-3 变压器的零序等值电路及其参数

4. 自耦变压器的零序等值电路及其参数



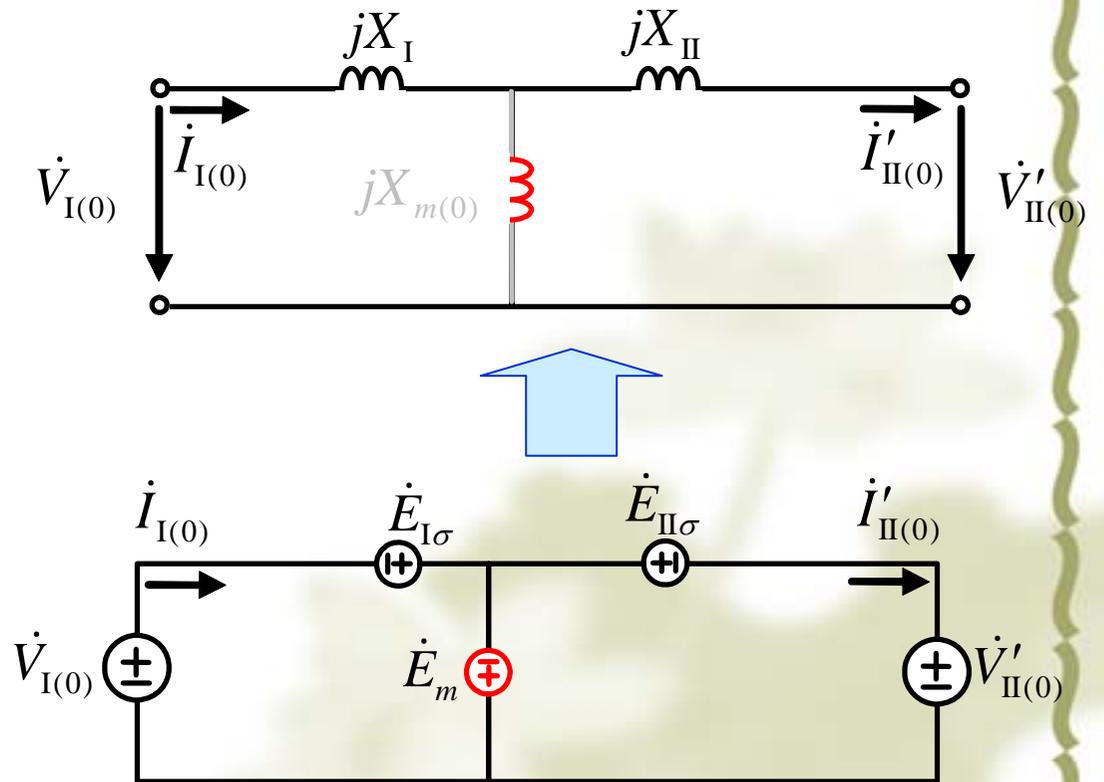
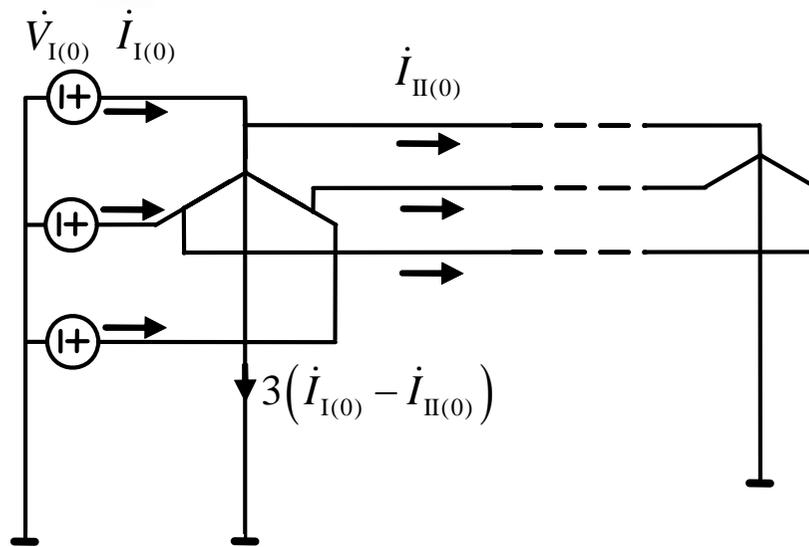
自耦变压器的特点：

- (1) 原副方之间有直接的电气联系；
- (2) 中性点入地电流取决于原副方零序电流
- (3) 中性点接地阻抗对各侧绕组零序参数均有影响；
- (4) 中性点不接地也可能通过零序电流

4. 自耦变压器的零序等值电路及其参数

(1) 中性点直接接地的双绕组自耦变压器

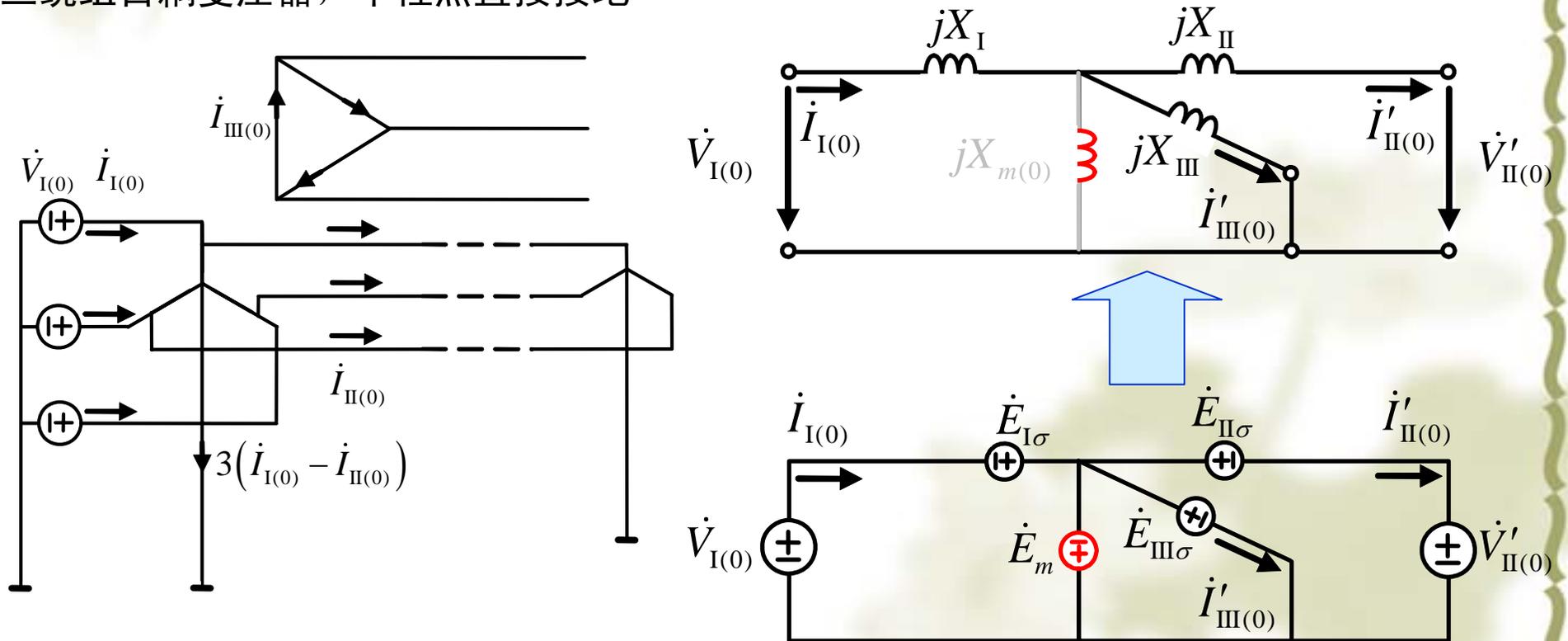
双绕组自耦变压器，中性点直接接地



4. 自耦变压器的零序等值电路及其参数

(2) 中性点直接接地的三绕组自耦变压器

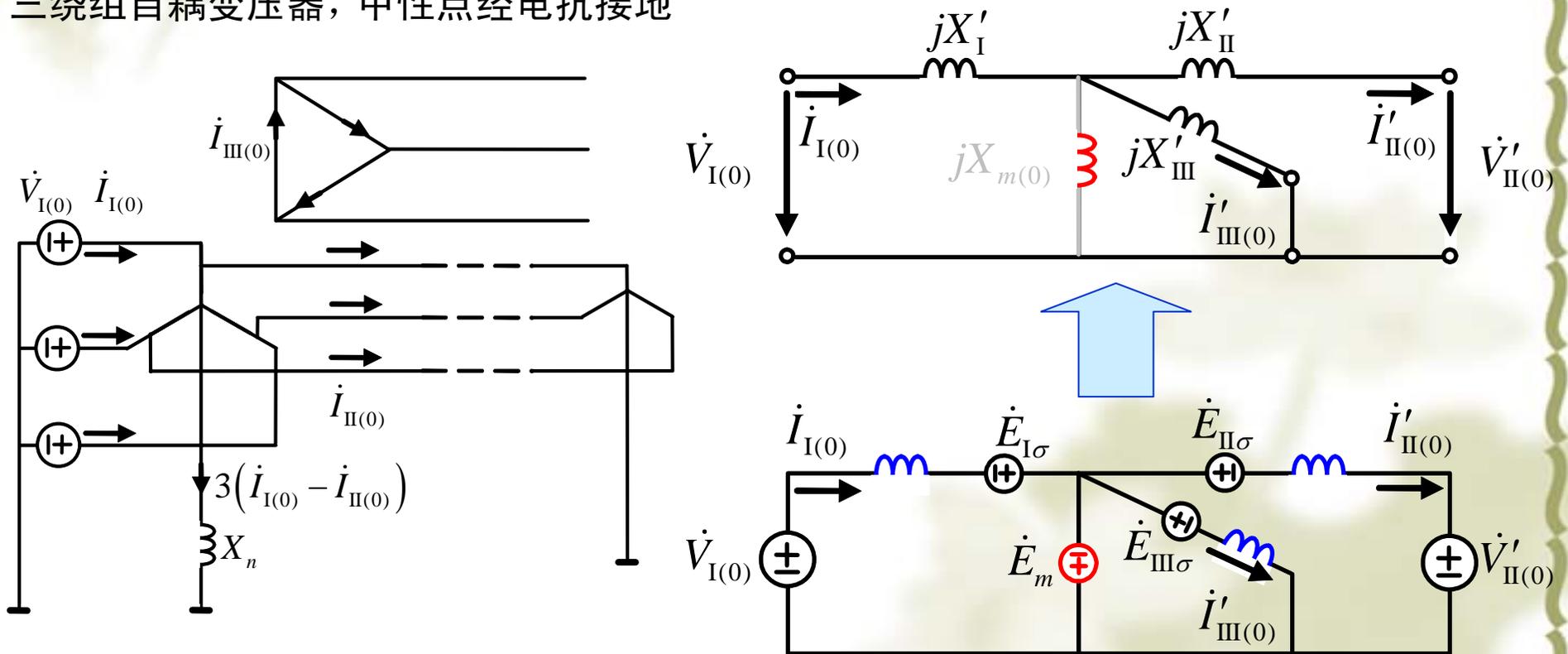
三绕组自耦变压器，中性点直接接地



4. 自耦变压器的零序等值电路及其参数

(3) 中性点经电抗接地的三绕组自耦变压器

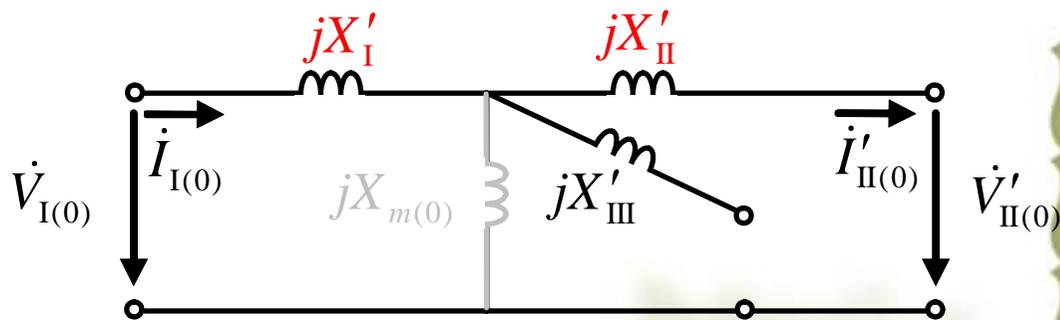
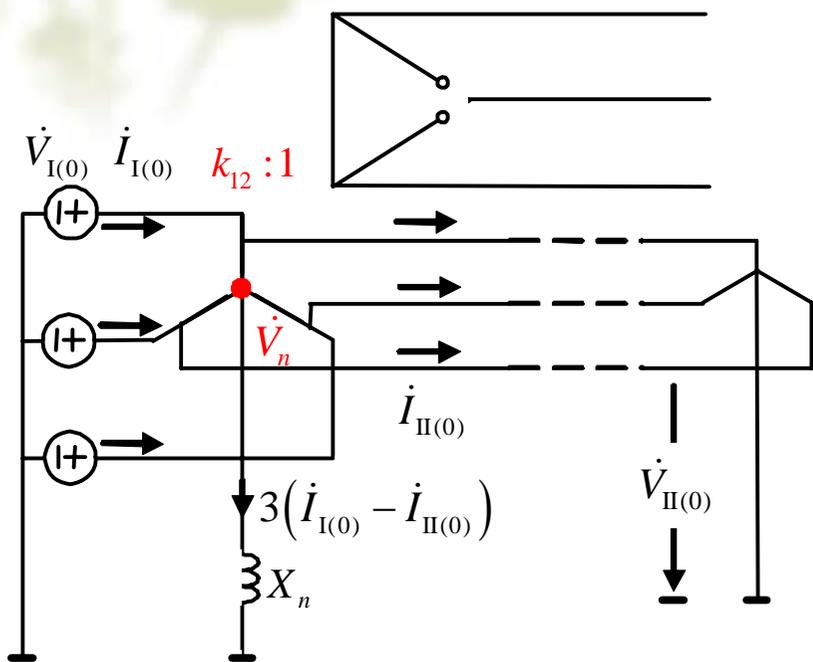
三绕组自耦变压器，中性点经电抗接地



4. 自耦变压器的零序等值电路及其参数

(3) 中性点经电抗接地的三绕组自耦变压器

三绕组自耦变压器，三角侧绕组开路



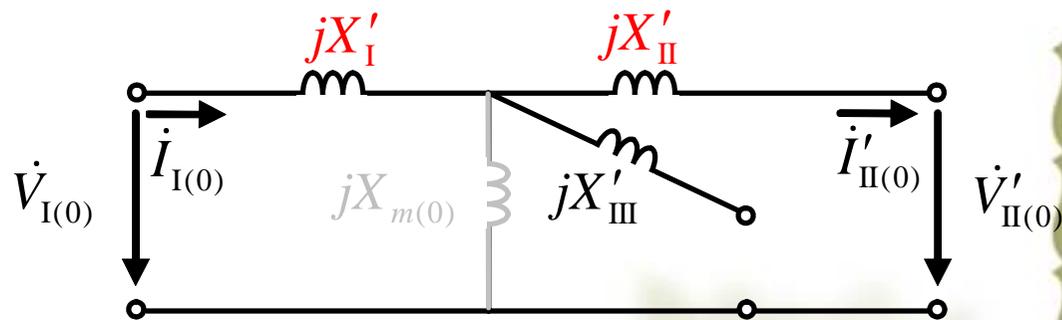
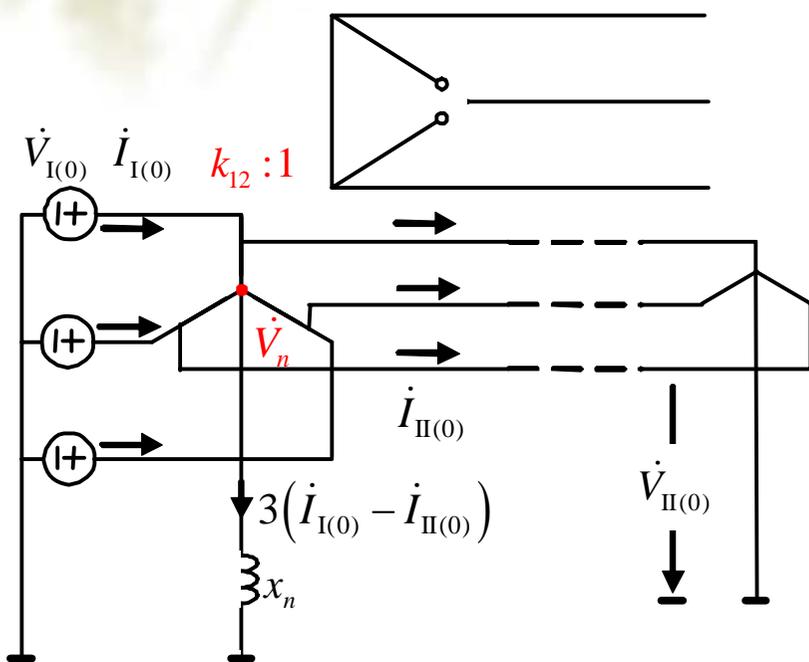
$$\begin{aligned} \dot{V}_{I(0)} &= \dot{V}_{In} + \dot{V}_n, \quad \dot{V}_{II(0)} = \dot{V}_{II_n} + \dot{V}_n \\ \dot{V}_n &= 3x_n (\dot{I}_{I(0)} - \dot{I}_{II(0)}) = 3x_n (1 - k_{12}) \dot{I}_{I(0)} \end{aligned}$$

$$\begin{aligned} j(X'_I + X'_{II}) &= \frac{\dot{V}_{I(0)} - \dot{V}'_{II(0)}}{\dot{I}_{I(0)}} \\ &= \frac{(\dot{V}_{In} + \dot{V}_n) - k_{12}(\dot{V}_{II_n} + \dot{V}_n)}{\dot{I}_{I(0)}} \\ &= \frac{\dot{V}_{In} - k_{12}\dot{V}_{II_n}}{\dot{I}_{I(0)}} + \frac{(1 - k_{12})\dot{V}_n}{\dot{I}_{I(0)}} \end{aligned}$$

4. 自耦变压器的零序等值电路及其参数

(3) 中性点经电抗接地的三绕组自耦变压器

三绕组自耦变压器，三角侧绕组开路



$$j(X'_I + X'_II) = jX_I + jX_{II} + j3x_n(1 - k_{12})^2$$

$$j(X'_I + X'_II) = \frac{\dot{V}_{In} - k_{12}\dot{V}_{IIIn}}{\dot{I}_{I(0)}} + \frac{(1 - k_{12})\dot{V}_n}{\dot{I}_{I(0)}}$$

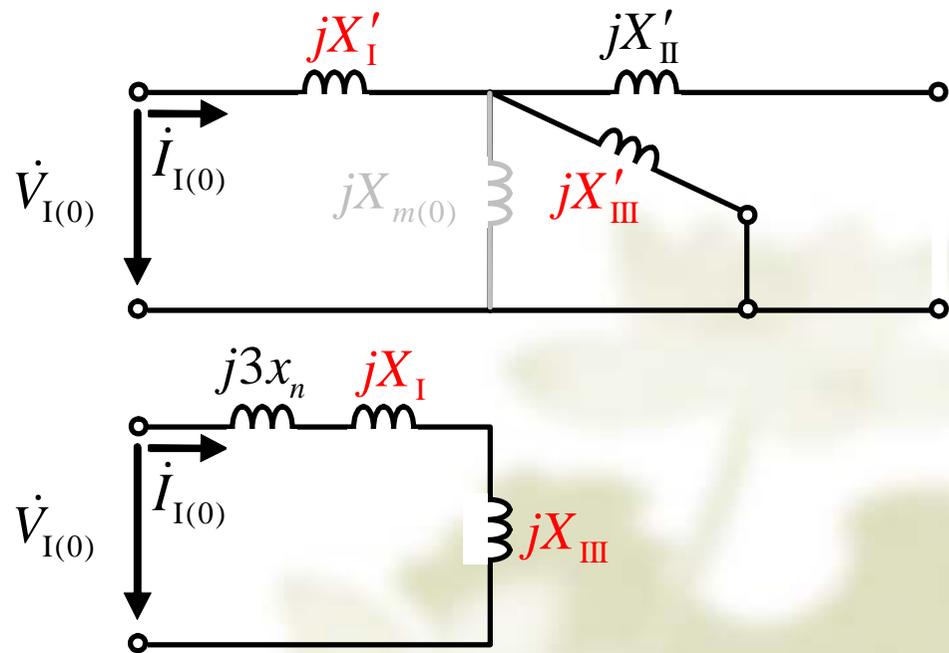
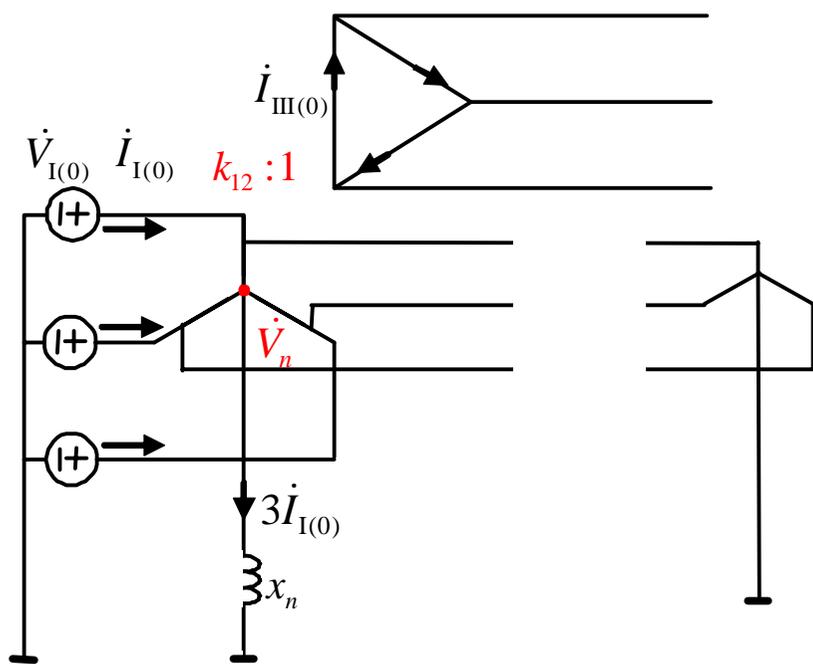
$$\dot{V}_n = 3x_n(\dot{I}_{I(0)} - \dot{I}_{II(0)}) = 3x_n(1 - k_{12})\dot{I}_{I(0)}$$

$$j(X_I + X_{II}) = \frac{\dot{V}_{In} - k_{12}\dot{V}_{IIIn}}{\dot{I}_{I(0)}}$$

4. 自耦变压器的零序等值电路及其参数

(3) 中性点经电抗接地的三绕组自耦变压器

三绕组自耦变压器，二次侧绕组开路

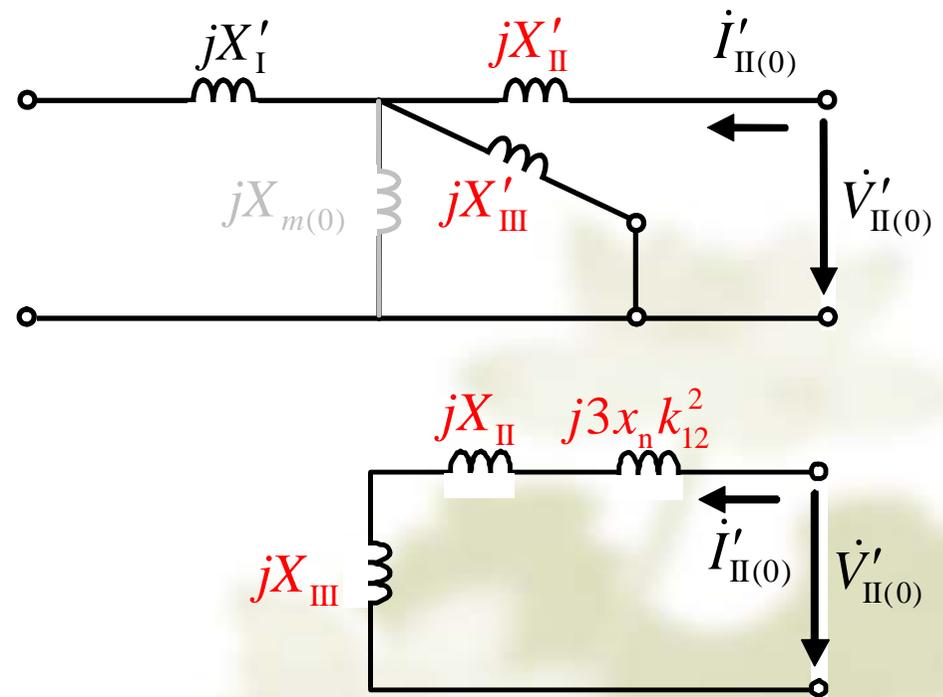
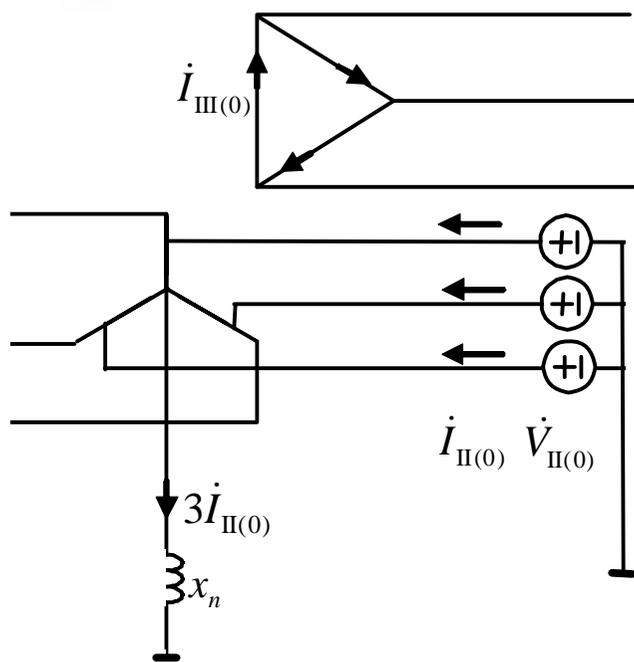


$$j(X'_I + X'_{III}) = jX_I + jX_{III} + j3x_n$$

4. 自耦变压器的零序等值电路及其参数

(3) 中性点经电抗接地的三绕组自耦变压器

三绕组自耦变压器，一次侧绕组开路



$$j(X'_{II} + X'_{III}) = jX_{II} + jX_{III} + j3x_n k_{12}^2$$

4. 自耦变压器的零序等值电路及其参数

(3) 中性点经电抗接地的三绕组自耦变压器

$$j(X'_I + X'_II) = jX_I + jX_{II} + j3x_n(1 - k_{12})^2$$

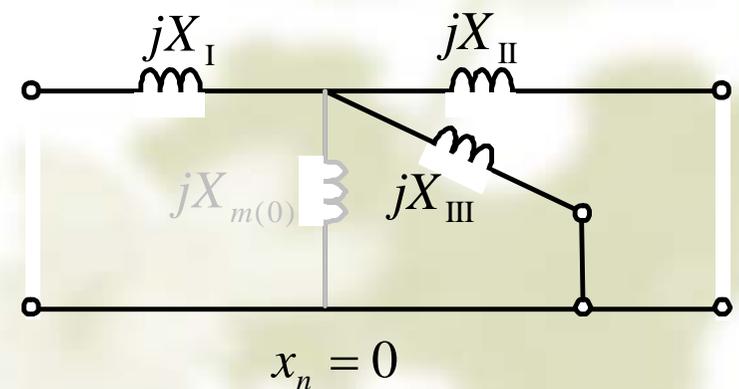
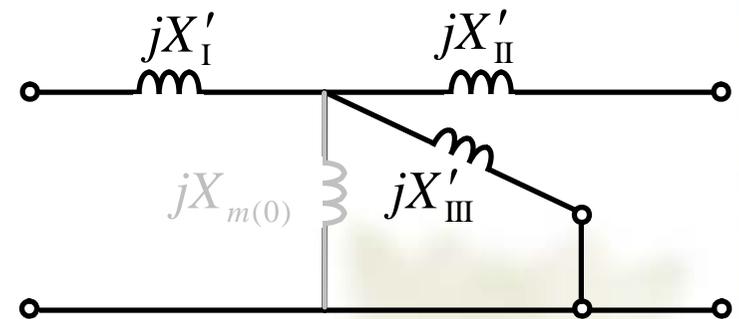
$$j(X'_I + X'_III) = jX_I + jX_{III} + j3x_n$$

$$j(X'_II + X'_III) = jX_{II} + jX_{III} + j3x_n k_{12}^2$$

$$jX'_I = jX_I + j3x_n(1 - k_{12})$$

$$jX'_II = jX_{II} + j3x_n k_{12}(1 - k_{12})$$

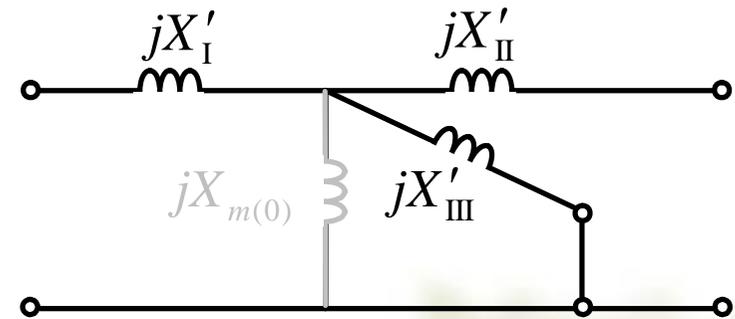
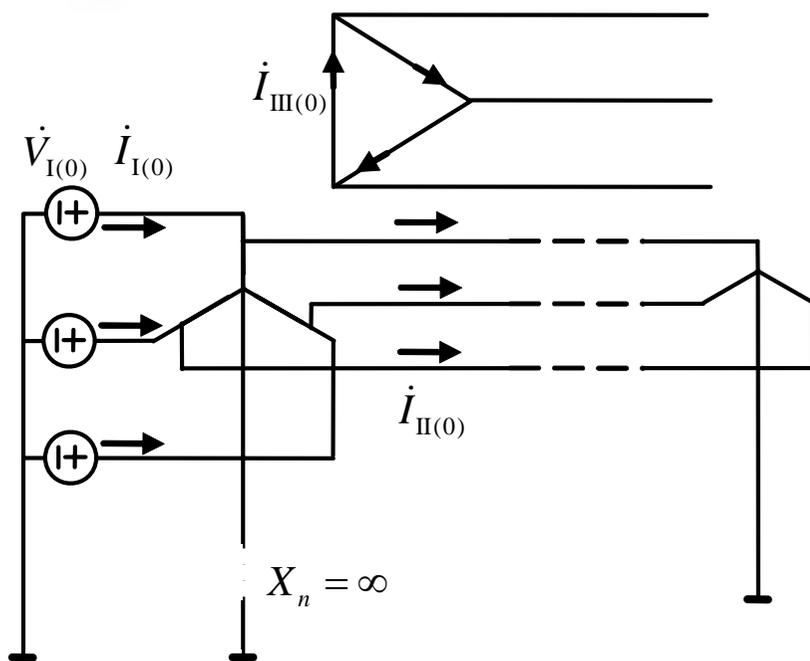
$$jX'_III = jX_{III} + j3x_n k_{12}$$



4. 自耦变压器的零序等值电路及其参数

(4) 中性点不接地的三绕组自耦变压器

三绕组自耦变压器，中性点不接地

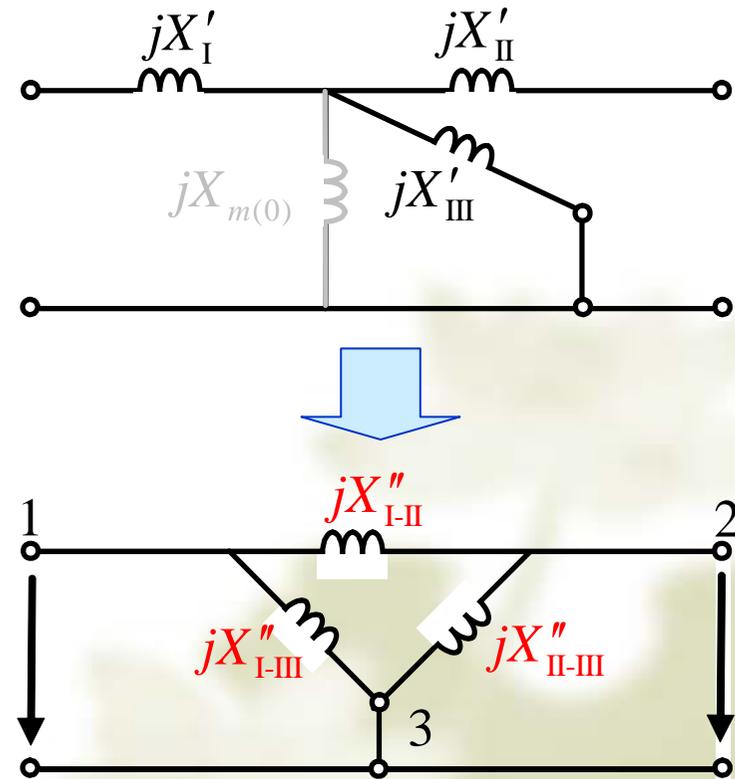
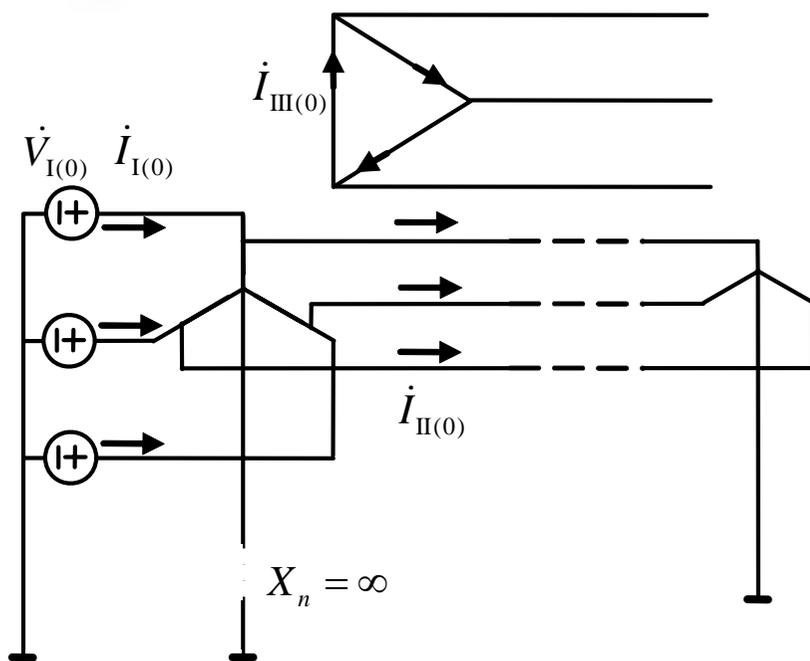


$$\begin{aligned}jX'_I &= jX_I + j3x_n(1 - k_{12}) \\jX'_II &= jX_I + j3x_n k_{12}(1 - k_{12}) \\jX'_III &= jX_{III} + j3x_n k_{12}\end{aligned}$$

4. 自耦变压器的零序等值电路及其参数

(4) 中性点不接地的三绕组自耦变压器

三绕组自耦变压器，中性点不接地



$$jX''_{I-II} + jX''_{I-III} + jX''_{II-III} = 0$$

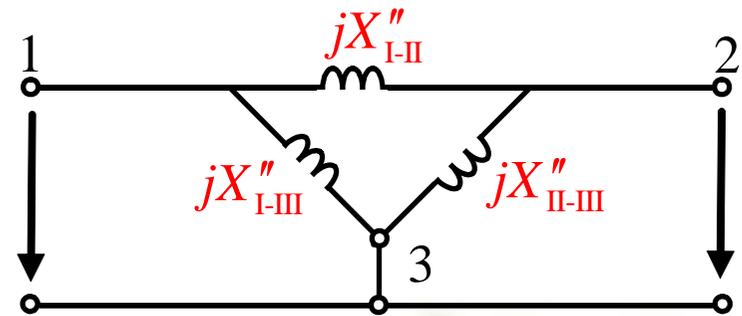
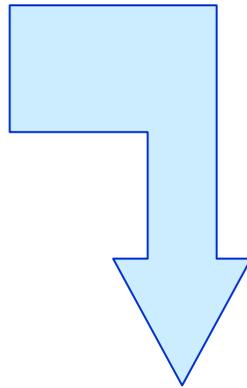
4. 自耦变压器的零序等值电路及其参数

(4) 中性点不接地的三绕组自耦变压器

$$jX'_I = jX_I + j3x_n(1-k_{12})$$

$$jX'_{II} = jX_I + j3x_n k_{12}(1-k_{12})$$

$$jX'_{III} = jX_{III} + j3x_n k_{12}$$



$$jX'_{I-II} = \lim_{x_n \rightarrow \infty} \left(jX'_I + jX'_{II} + \frac{jX'_I \times jX'_{II}}{jX'_{III}} \right) = k_{12} X_I + \frac{1}{k_{12}} X_{II} + \frac{(1-k_{12})^2}{k_{12}} X_{III}$$

$$jX'_{I-III} = \lim_{x_n \rightarrow \infty} \left(jX'_I + jX'_{III} + \frac{jX'_I \times jX'_{III}}{jX'_{II}} \right) = -\frac{k_{12}}{1-k_{12}} X_I - \frac{1}{k_{12}(1-k_{12})} X_{II} - \frac{1-k_{12}}{k_{12}} X_{III}$$

$$jX'_{II-III} = \lim_{x_n \rightarrow \infty} \left(jX'_{II} + jX'_{III} + \frac{jX'_{II} \times jX'_{III}}{jX'_I} \right) = \frac{k_{12}^2}{1-k_{12}} X_I + \frac{1}{(1-k_{12})} X_{II} + (1-k_{12}) X_{III}$$

7-4 架空输电线的零序阻抗及其等值电路

1. 单导线—大地回路的自阻抗

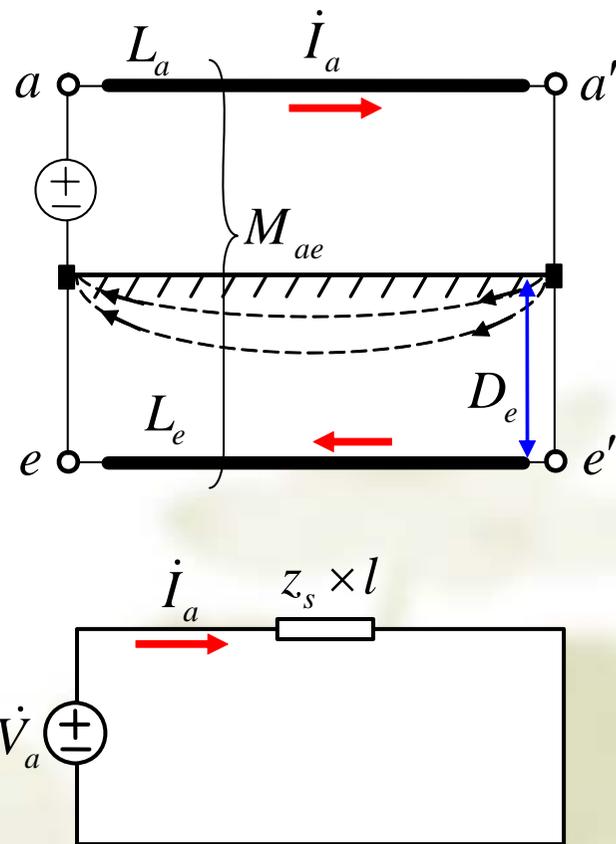
自阻抗: 单导线以大地为回路时对应于单位长度导线的回路阻抗

$$\{L\}_{\text{H/m}} = \frac{\mu_0}{2\pi} \left[\ln \frac{2l}{D_s} - 1 \right]$$

$$\{M\}_{\text{H/m}} = \frac{\mu_0}{2\pi} \left[\ln \frac{2l}{D} - 1 \right]$$

$$\{L_S\}_{\text{H/m}} = L_a + L_e - 2M_{ae} = 2 \times 10^{-7} \ln \frac{D_e}{D_s}$$

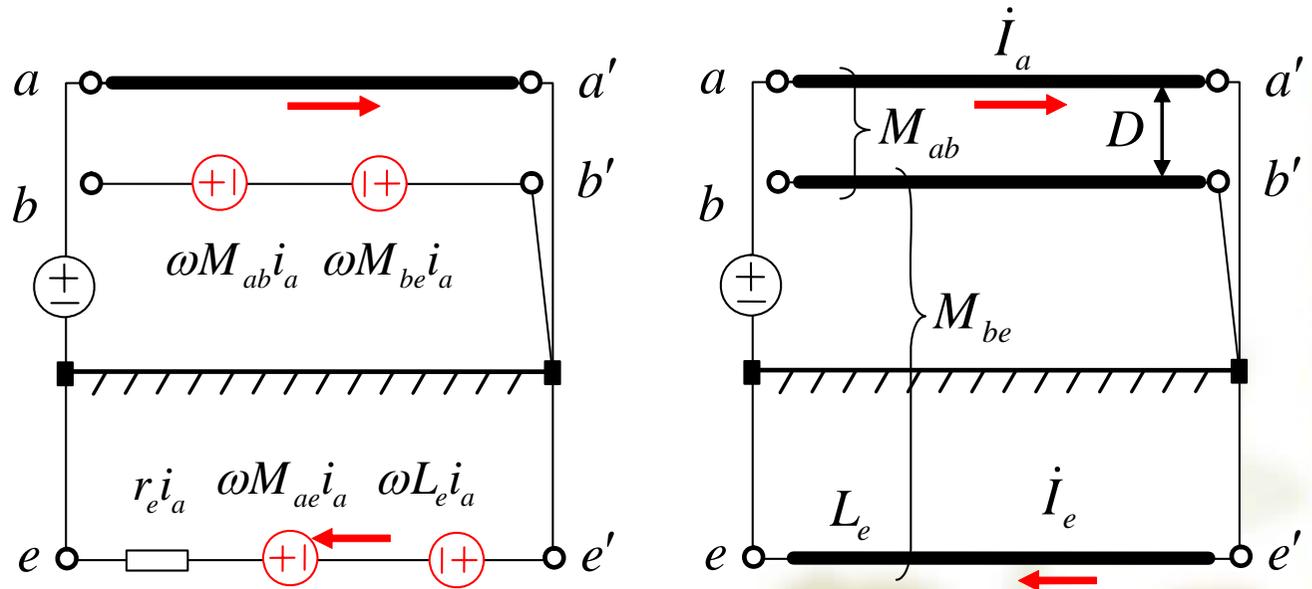
$$\{z_S\}_{\Omega/\text{km}} = r_a + r_e + j\omega L_S = r_a + r_e + j0.1445 \lg \frac{D_e}{D_s}$$



7-4 架空输电线的零序阻抗及其等值电路

2. 两平行单导线—大地回路间的互阻抗

互阻抗: 一个回路通过单位电流时, 在另一个回路单位长度上产生的压降



$$\psi_{bb'} = (M_{ab} - M_{be}) i_a$$

$$\psi_{ee'} = (M_{ae} - L_e) i_a$$

$$\left\{ \Delta \dot{E} \right\}_{\Omega/\text{km}} = j\omega [M_{ab} - M_{be} + L_e - M_{ae}] \dot{I}_a$$

$$\left\{ z_m \right\}_{\Omega/\text{km}} = r_e + j\omega (M_{ab} - M_{be} - M_{ae} + L_e) = r_e + j0.1445 \lg \frac{D_e}{D}$$

7-4 架空输电线的零序阻抗及其等值电路

3. 三相输电线路的一相等值零序阻抗

$$\dot{V}_a = z_s \dot{I}_a + z_m \dot{I}_b + z_m \dot{I}_c$$

$$\dot{V}_{a(1)} = (z_s - z_m) \dot{I}_{a(1)}$$

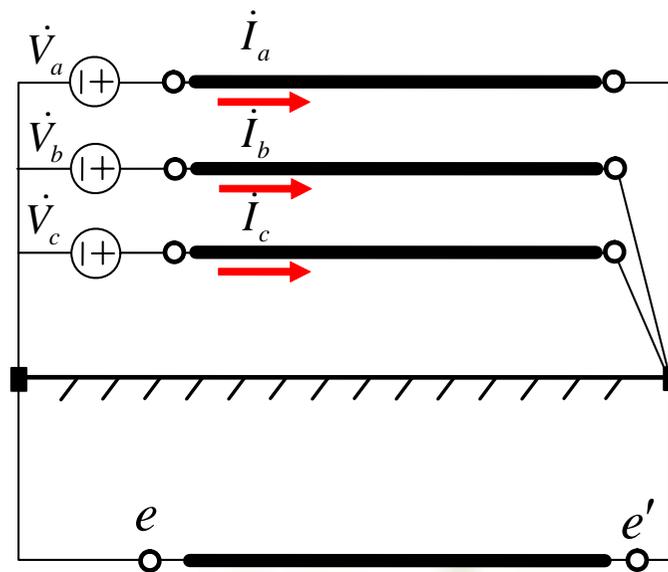
$$\dot{V}_{a(2)} = (z_s - z_m) \dot{I}_{a(2)}$$

$$\dot{V}_{a(0)} = (z_s + 2z_m) \dot{I}_{a(0)}$$

$$z_{(1)} = z_s - z_m$$

$$z_{(2)} = z_s - z_m$$

$$z_{(0)} = z_s + 2z_m$$



$$\left\{ z_{(0)} \right\}_{\Omega/\text{km}} = r_a + 3r_e + j0.4335 \lg \frac{D_e}{D_{ST}}$$

7-4 架空输电线的零序阻抗及其等值电路

3. 三相输电线路的一相等值零序阻抗

$$\dot{V}_a = z_s \dot{I}_a + z_m \dot{I}_b + z_m \dot{I}_c$$

$$\dot{V}_{a(1)} = (z_s - z_m) \dot{I}_{a(1)}$$

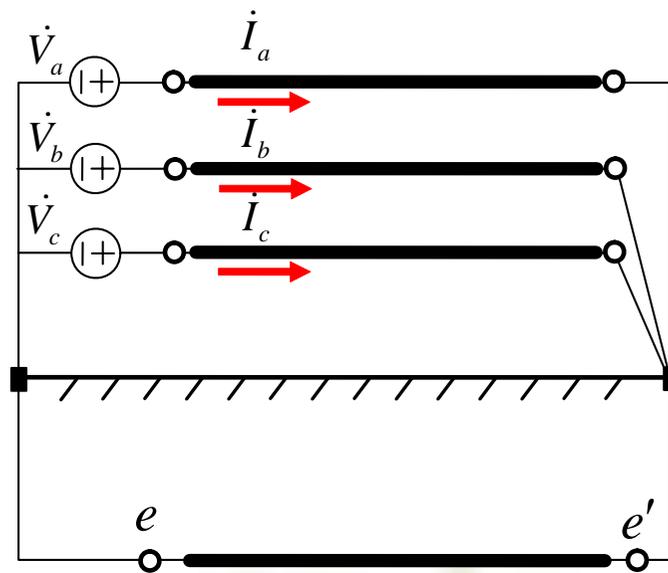
$$\dot{V}_{a(2)} = (z_s - z_m) \dot{I}_{a(2)}$$

$$\dot{V}_{a(0)} = (z_s + 2z_m) \dot{I}_{a(0)}$$

$$z_{(1)} = z_s - z_m$$

$$z_{(2)} = z_s - z_m$$

$$z_{(0)} = z_s + 2z_m$$



$$\{L_S\}_{\text{H/m}} = L_a + L_e - 2M_{ae}$$

$$\{z_{(0)}\}_{\Omega/\text{km}} = r_a + 3r_e + j0.4335 \lg \frac{D_e}{D_{ST}}$$

$$\{z_S\}_{\Omega/\text{km}} = r_a + r_e + j\omega L_S$$

$$\{z_m\}_{\Omega/\text{km}} = r_e + j\omega (M_{ab} - M_{be} - M_{ae} + L_e)$$

7-4 架空输电线的零序阻抗及其等值电路

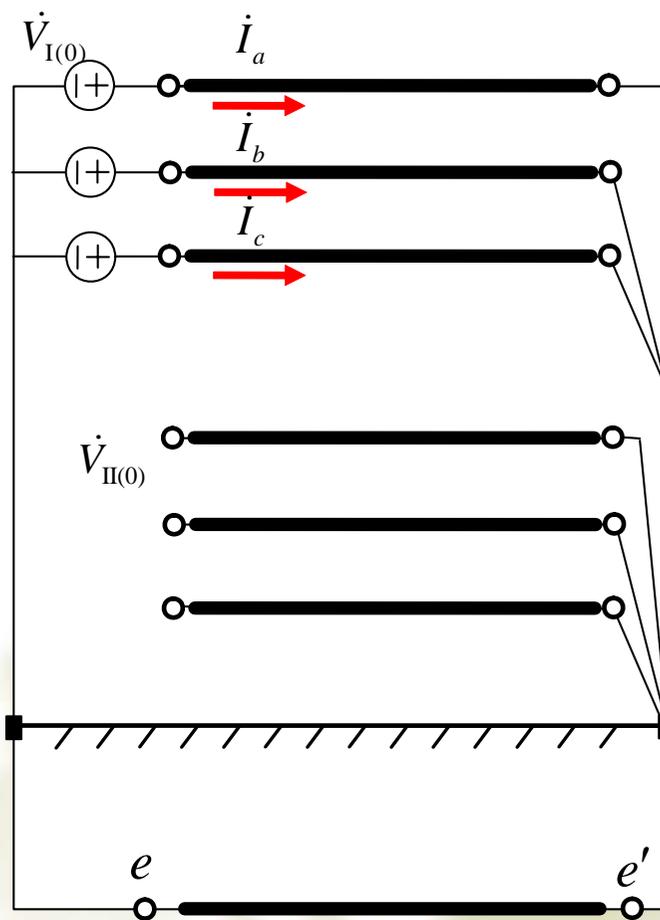
4. 平行架设双回输电线路的零序阻抗及等值电路

(1) 线路零序参数

$$\left\{ z_{I(0)} \right\}_{\Omega/\text{km}} = r_a + 3r_e + j0.4335 \lg \frac{D_e}{D_{ST}}$$

$$\left\{ z_{I-II(0)} \right\}_{\Omega/\text{km}} = 3 \left[r_e + j0.1445 \lg \frac{D_e}{D_{I-II}} \right]$$

互阻抗的求法 $Z_{I-II(0)}$: I回输电线路三相通过单位零序电流 $\dot{i}_{I(0)}$, 在II回每相产生的电压降落在数值上即为 $Z_{I-II(0)}$



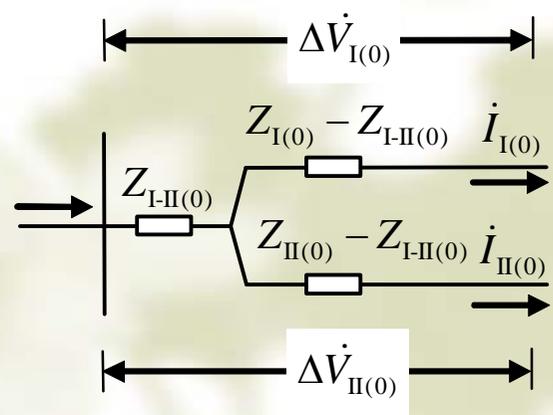
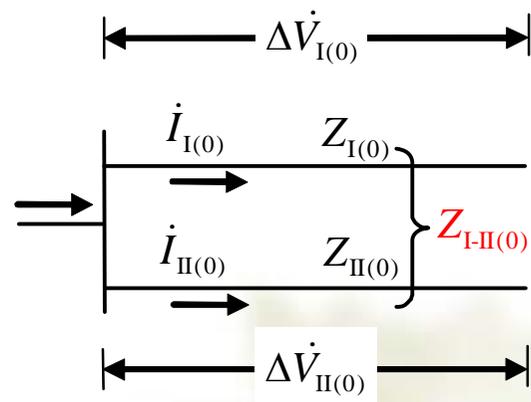
7-4 架空输电线的零序阻抗及其等值电路

4. 平行架设双回输电线路的零序阻抗及等值电路

(2) 平行架设双回输电线路的零序等值电路 (首端相连)

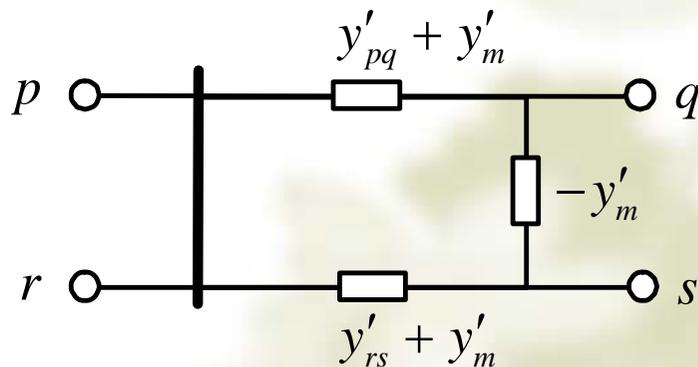
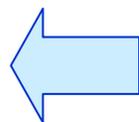
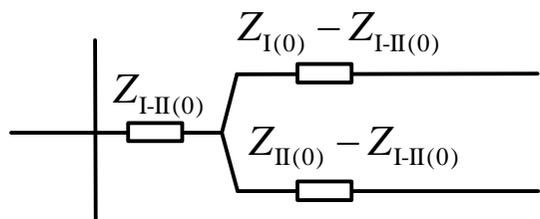
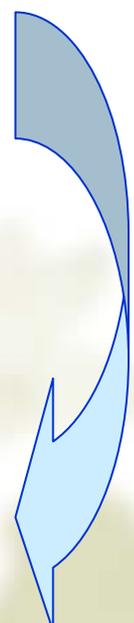
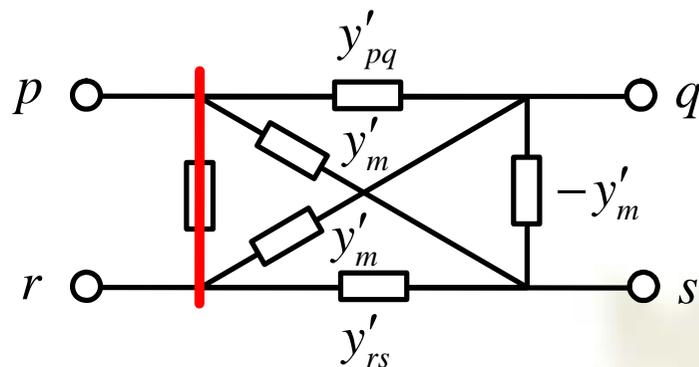
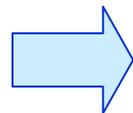
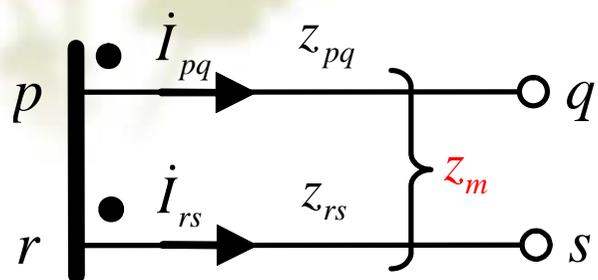
$$\begin{aligned} \dot{V}_{I(0)} &= Z_{I(0)} \dot{I}_{I(0)} + Z_{I-II(0)} \dot{I}_{II(0)} \\ \dot{V}_{II(0)} &= Z_{I-II(0)} \dot{I}_{I(0)} + Z_{II(0)} \dot{I}_{II(0)} \end{aligned}$$

$$\begin{aligned} \dot{V}_{I(0)} &= Z_{I-II(0)} (\dot{I}_{I(0)} + \dot{I}_{II(0)}) + (Z_{I(0)} - Z_{I-II(0)}) \dot{I}_{I(0)} \\ \dot{V}_{II(0)} &= Z_{I-II(0)} (\dot{I}_{I(0)} + \dot{I}_{II(0)}) + (Z_{II(0)} - Z_{I-II(0)}) \dot{I}_{II(0)} \end{aligned}$$



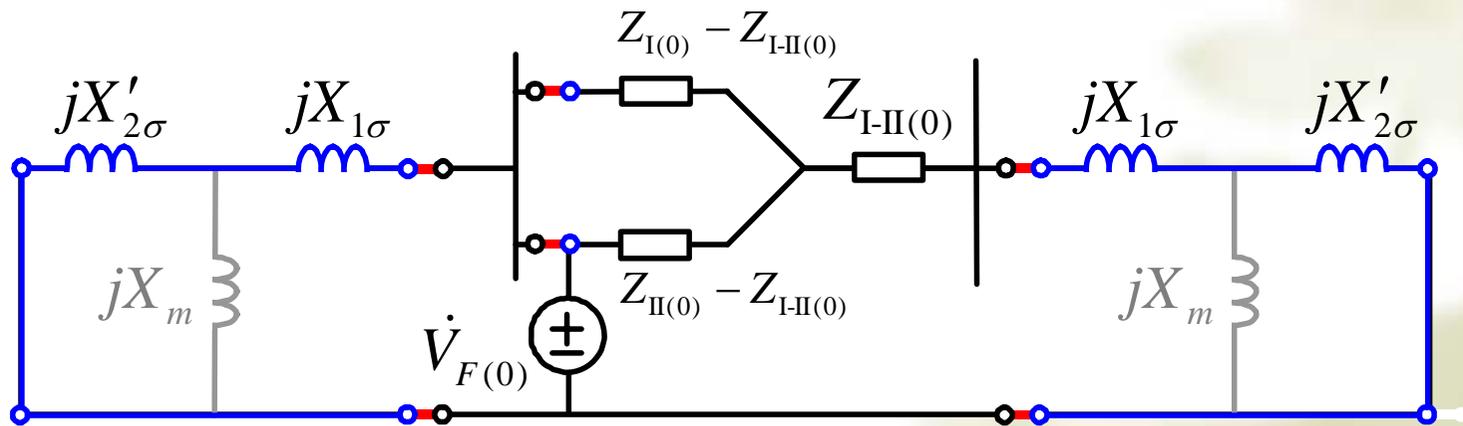
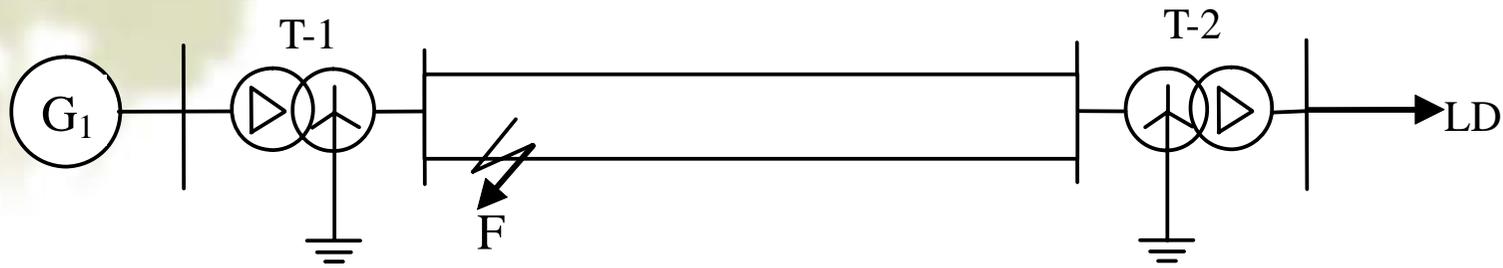
Review: 4-1 节点导纳矩阵

Y 阵的修改——一端互联的互感支路



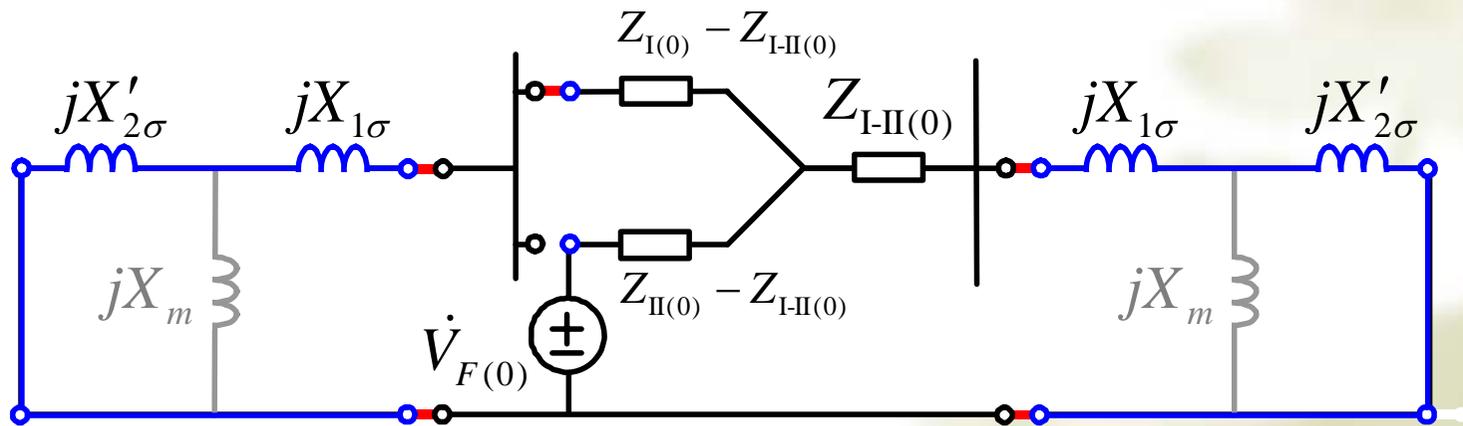
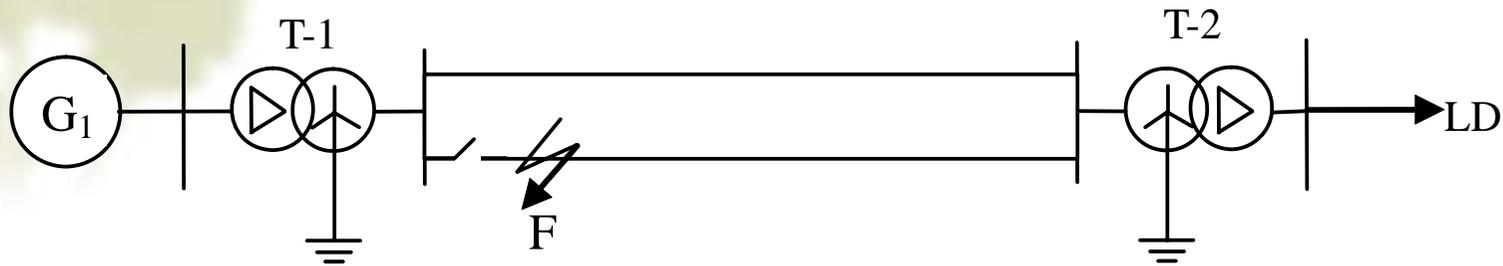
4. 平行架设双回输电线路的零序阻抗及等值电路

(2) 平行架设双回输电线路的零序等值电路——应用举例



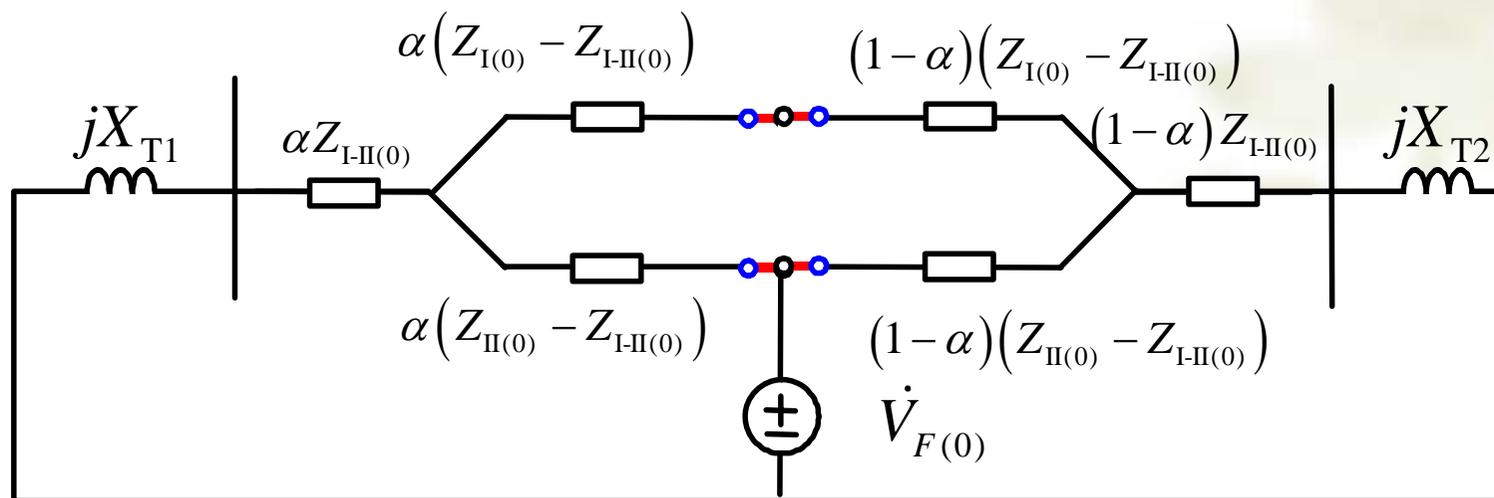
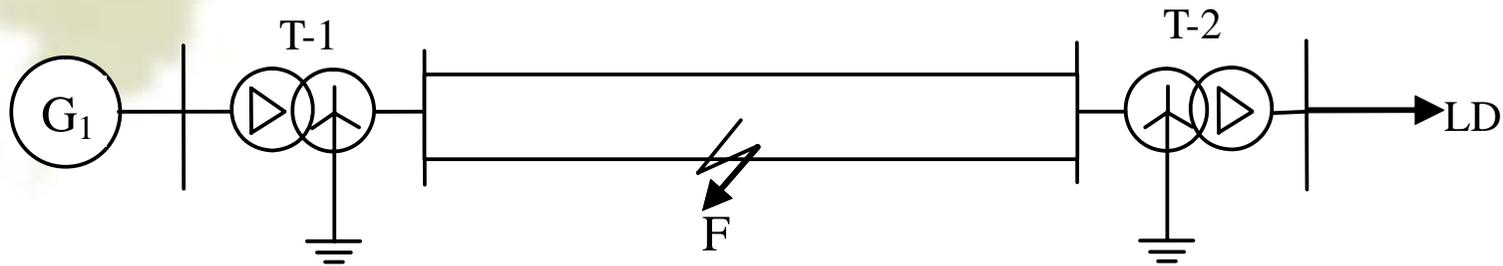
4. 平行架设双回输电线路的零序阻抗及等值电路

(2) 平行架设双回输电线路的零序等值电路——应用举例



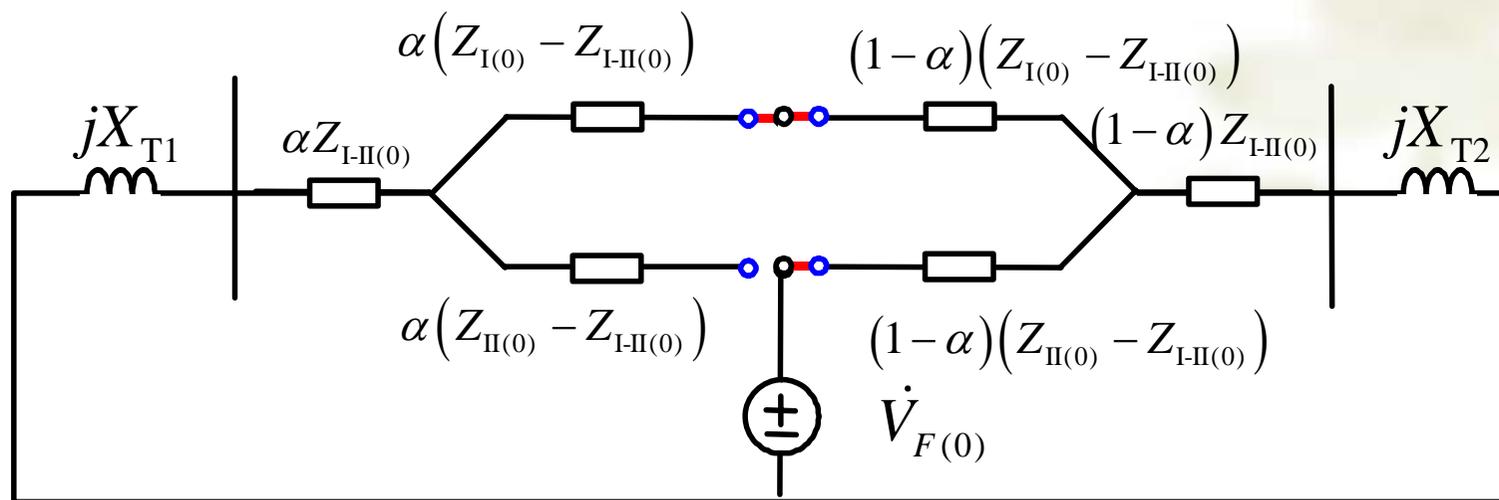
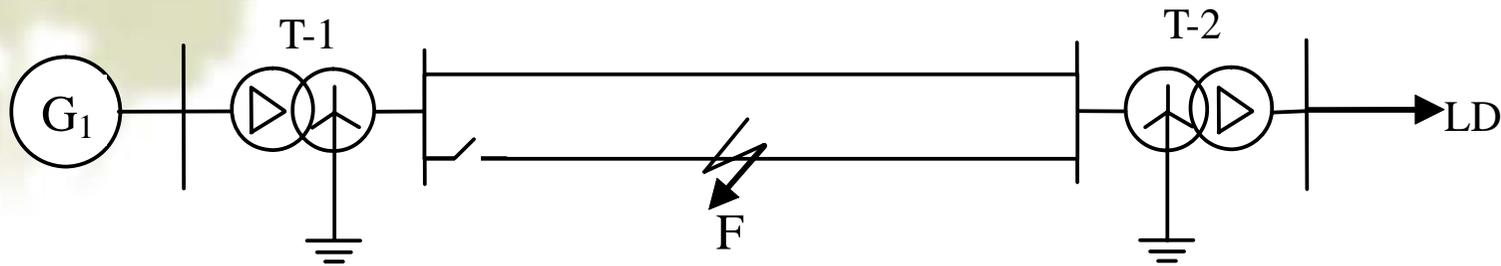
4. 平行架设双回输电线路的零序阻抗及等值电路

(2) 平行架设双回输电线路的零序等值电路——应用举例



4. 平行架设双回输电线路的零序阻抗及等值电路

(2) 平行架设双回输电线路的零序等值电路——应用举例

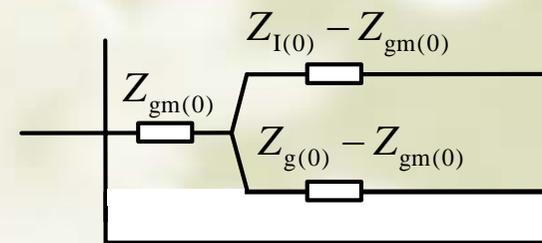
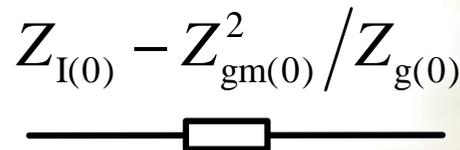
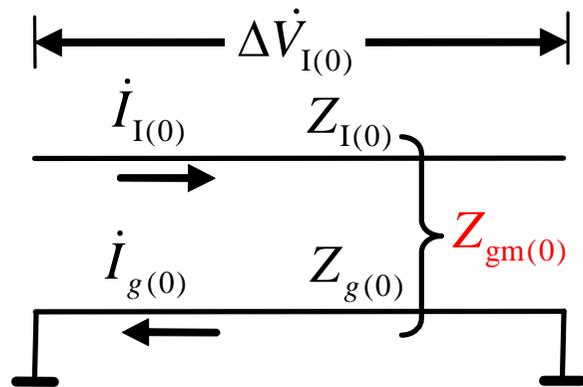
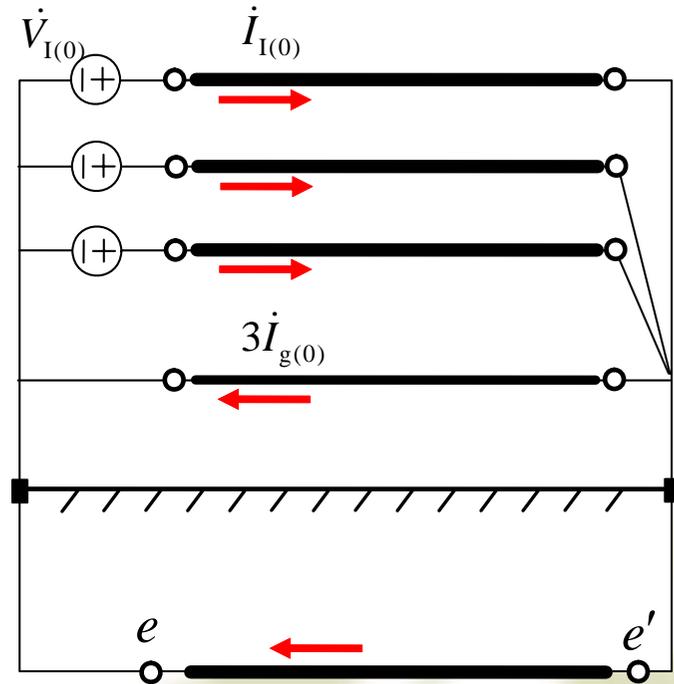


4. 平行架设双回输电线路的零序阻抗及等值电路

(3) 有架空地线的单回输电线路的零序等值电路

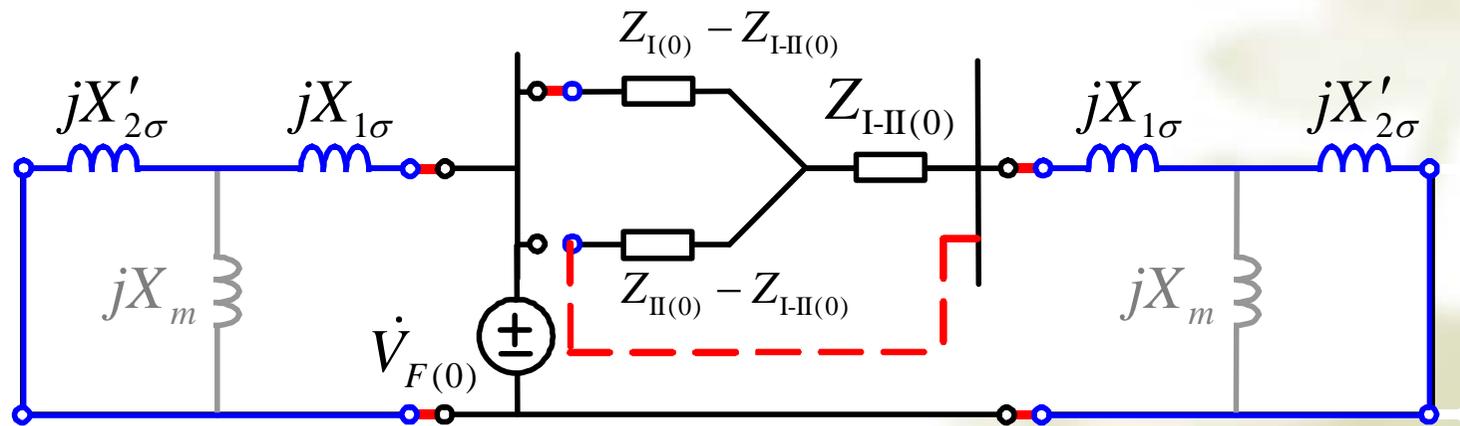
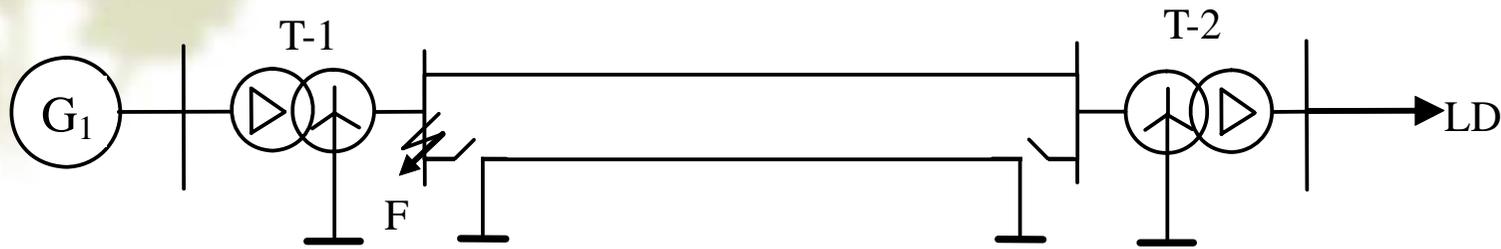
$$\begin{aligned} \Delta \dot{V}_{I(0)} &= Z_{I(0)} \dot{I}_{I(0)} - Z_{gm(0)} \dot{I}_{g(0)} \\ 0 &= Z_{g(0)} \dot{I}_{g(0)} - Z_{gm(0)} \dot{I}_{I(0)} \end{aligned}$$

$$\dot{V}_{I(0)} = \left(Z_{I(0)} - \frac{Z_{gm(0)}^2}{Z_{g(0)}} \right) \dot{I}_{I(0)}$$



4. 平行架设双回输电线路的零序阻抗及等值电路

(3) 平行架设双回输电线路，一回停电检修 — 应用举例



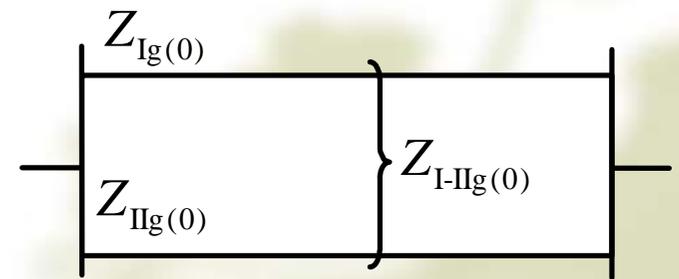
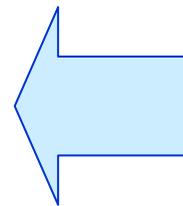
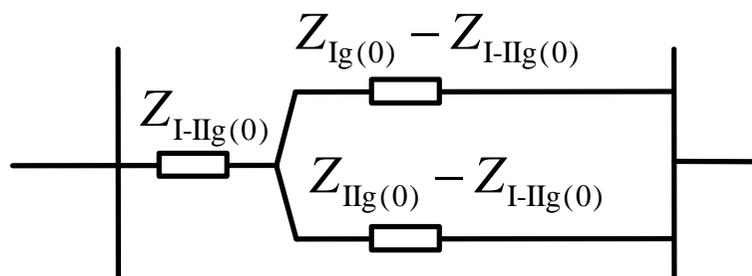
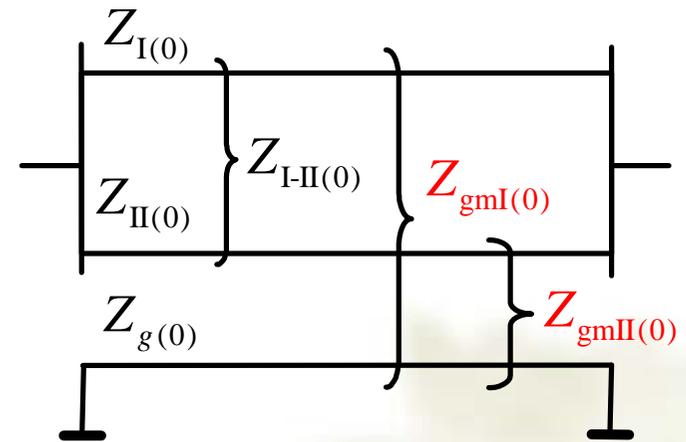
4. 平行架设双回输电线路的零序阻抗及等值电路

(3) 有架空地线的双回输电线路的零序等值电路

$$Z_{Ig(0)} = Z_{I(0)} - Z_{gmI(0)}^2 / Z_g(0)$$

$$Z_{IIg(0)} = Z_{II(0)} - Z_{gmII(0)}^2 / Z_g(0)$$

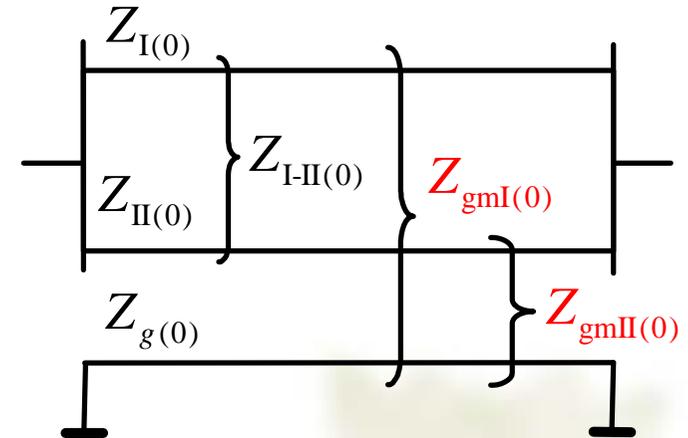
$$Z_{I-IIg(0)} = Z_{I-II(0)} - (Z_{gmI(0)} \times Z_{gmII(0)}) / Z_g(0)$$



4. 平行架设双回输电线路的零序阻抗及等值电路

(3) 有架空地线的双回输电线路的零序等值电路

$$\begin{aligned}\Delta \dot{V}_{I(0)} &= Z_{I(0)} \dot{I}_{I(0)} + Z_{I-II(0)} \dot{I}_{II(0)} - Z_{gmI(0)} \dot{I}_{g(0)} \\ \Delta \dot{V}_{II(0)} &= Z_{II(0)} \dot{I}_{II(0)} + Z_{I-II(0)} \dot{I}_{I(0)} - Z_{gmII(0)} \dot{I}_{g(0)} \\ 0 &= Z_{g(0)} \dot{I}_{g(0)} - Z_{gmI(0)} \dot{I}_{I(0)} - Z_{gmII(0)} \dot{I}_{II(0)}\end{aligned}$$

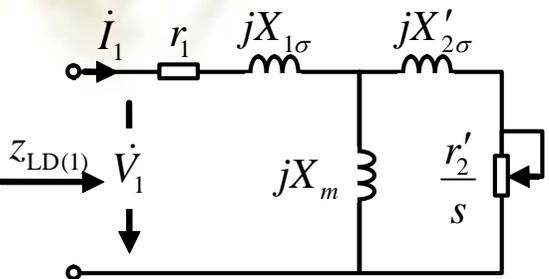
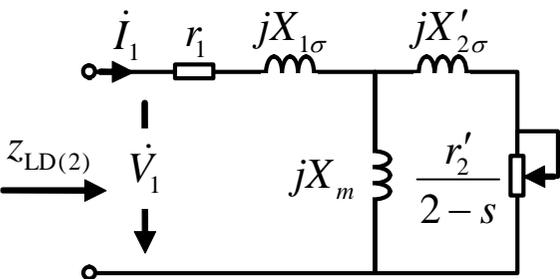
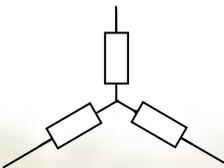


$$\begin{aligned}Z_{gmI(0)} \dot{I}_{g(0)} &= \left(Z_{gmI(0)}^2 / Z_{g(0)} \right) \dot{I}_{I(0)} + \left(Z_{gmI(0)} Z_{gmII(0)} / Z_{g(0)} \right) \dot{I}_{II(0)} \\ Z_{gmII(0)} \dot{I}_{g(0)} &= \left(Z_{gmI(0)} Z_{gmII(0)} / Z_{g(0)} \right) \dot{I}_{I(0)} + \left(Z_{gmII(0)}^2 / Z_{g(0)} \right) \dot{I}_{II(0)}\end{aligned}$$

$$\begin{aligned}\Delta \dot{V}_{I(0)} &= Z_{Ig(0)} \dot{I}_{I(0)} + Z_{I-IIg(0)} \dot{I}_{II(0)} \\ \Delta \dot{V}_{II(0)} &= Z_{IIg(0)} \dot{I}_{II(0)} + Z_{I-IIg(0)} \dot{I}_{I(0)}\end{aligned}$$

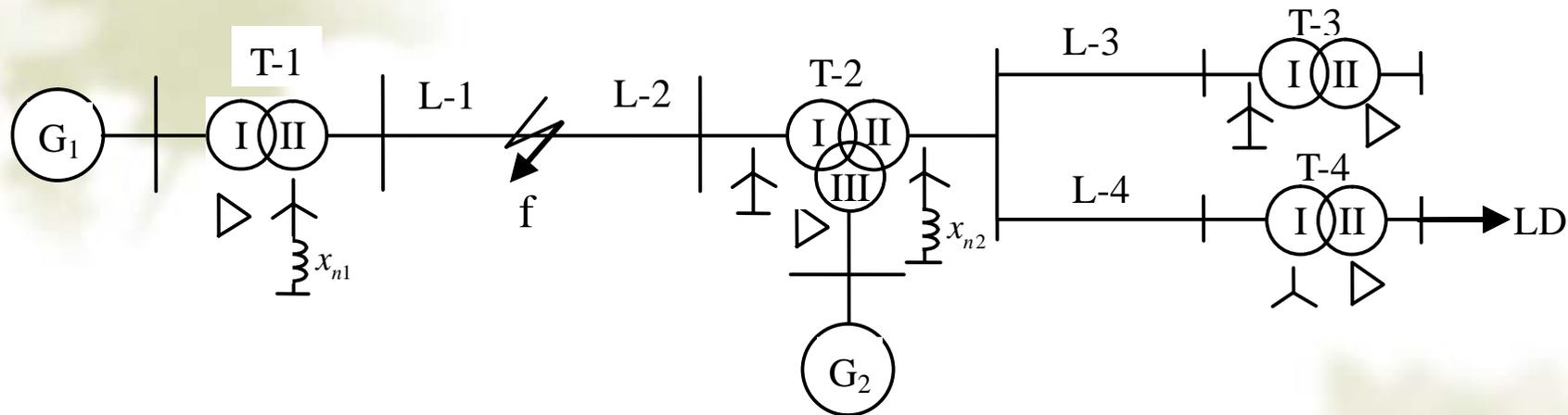
$$\begin{aligned}Z_{Ig(0)} &= Z_{I(0)} - Z_{gmI(0)}^2 / Z_{g(0)} \\ Z_{IIg(0)} &= Z_{II(0)} - Z_{gmII(0)}^2 / Z_{g(0)} \\ Z_{I-IIg(0)} &= Z_{I-II(0)} - \left(Z_{gmI(0)} \times Z_{gmII(0)} \right) / Z_{g(0)}\end{aligned}$$

7-6 综合负荷的序阻抗

正序阻抗	负序阻抗	零序阻抗
		
$z_{LD(1)} = \frac{V_{LD}^2}{S_{LD}} (\cos \varphi + j \sin \varphi)$		
$z_{LD(1)} = 0.8 + j0.6$ $z_{LD(1)} = j1.2$	$x_{(2)} = j0.35$	$x_{(0)} = \infty$

7-7 电力系统各序网络的制定

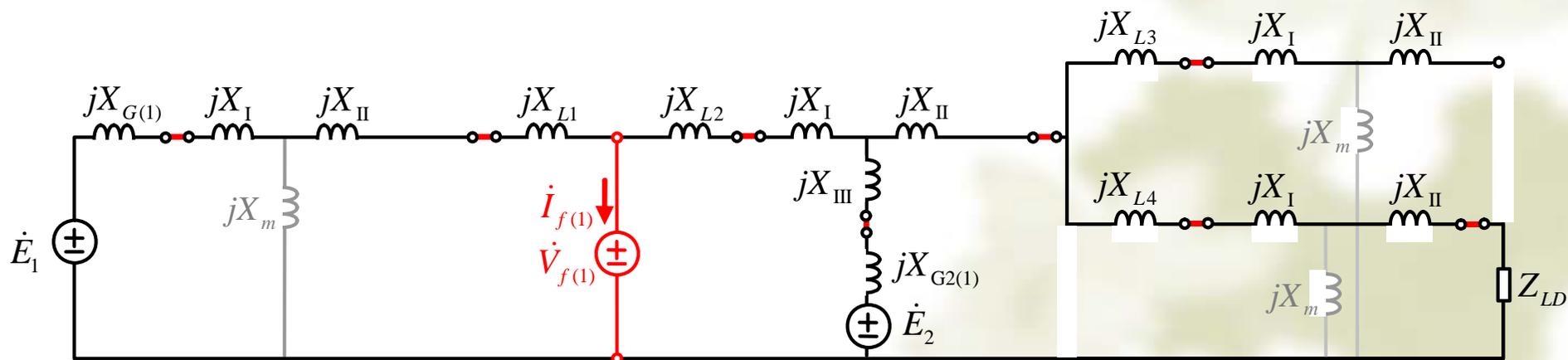
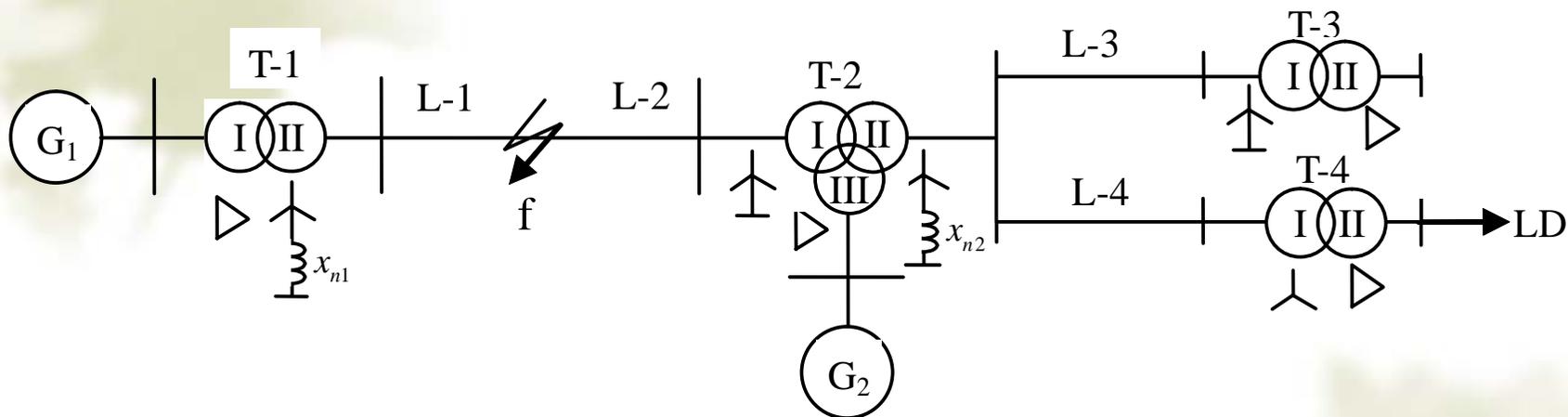
算例



- 在故障点分别叠加各序电势，从故障点开始，逐步查明各序电流流通的情况；
- 某一序电流能流通的元件，必须包括在该序网络中，并用相应的序参数和等值电路表示。

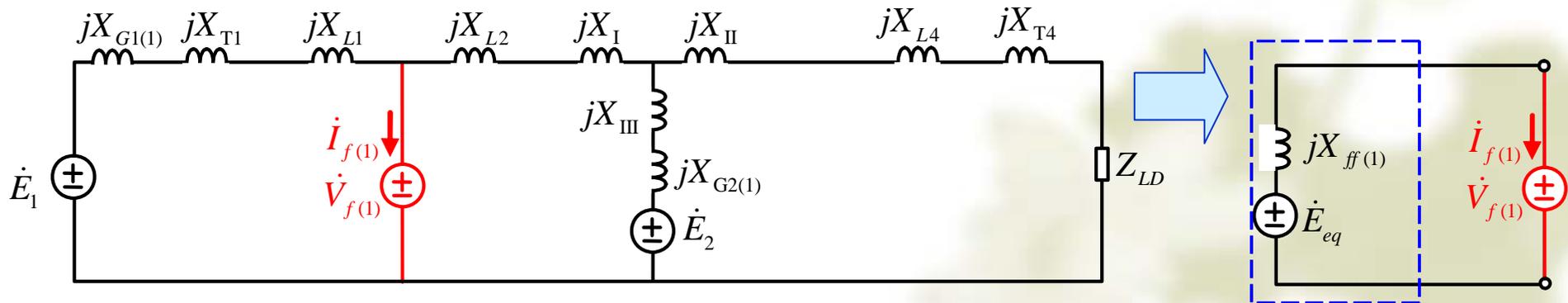
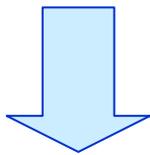
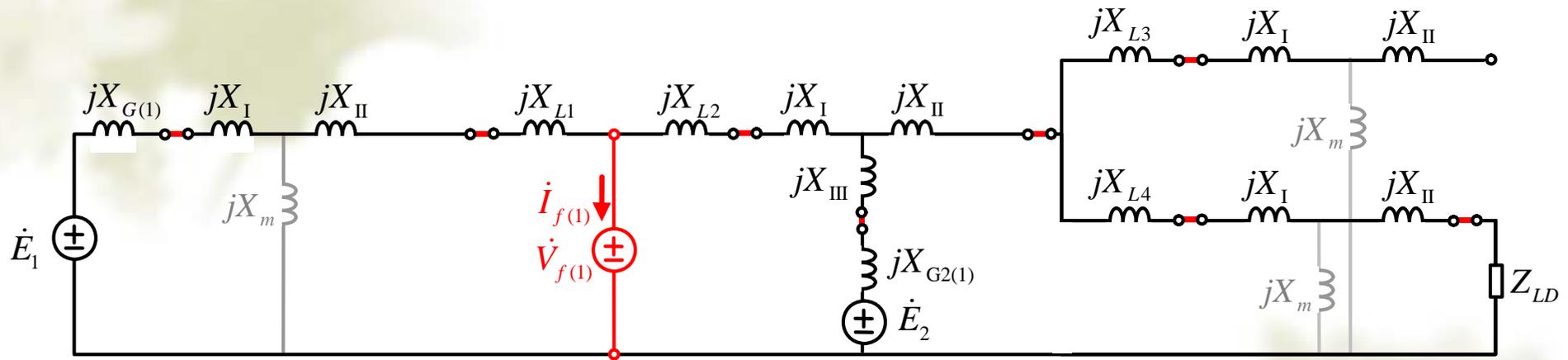
7-7 电力系统各序网络的制定

算例—正序网络



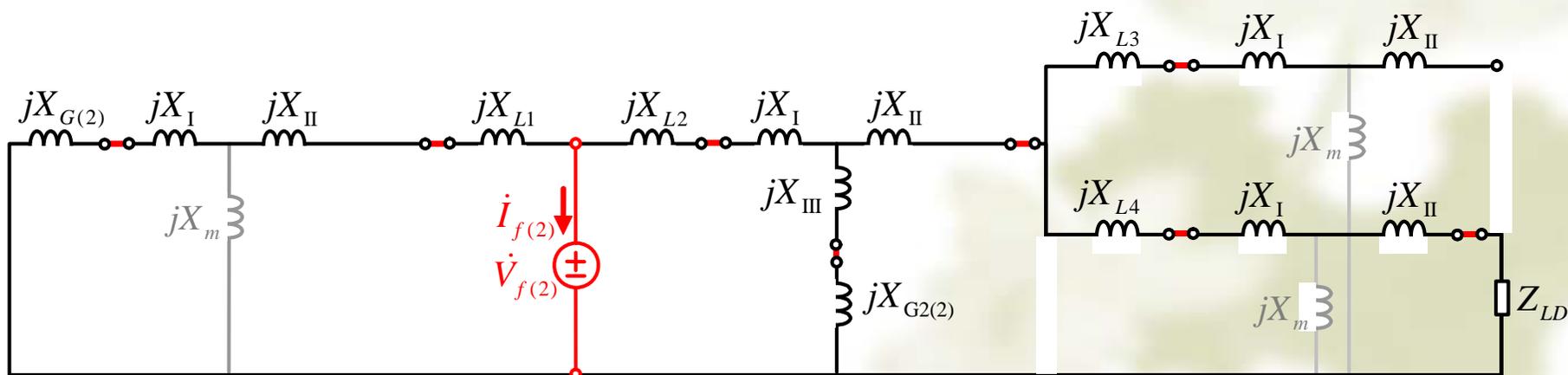
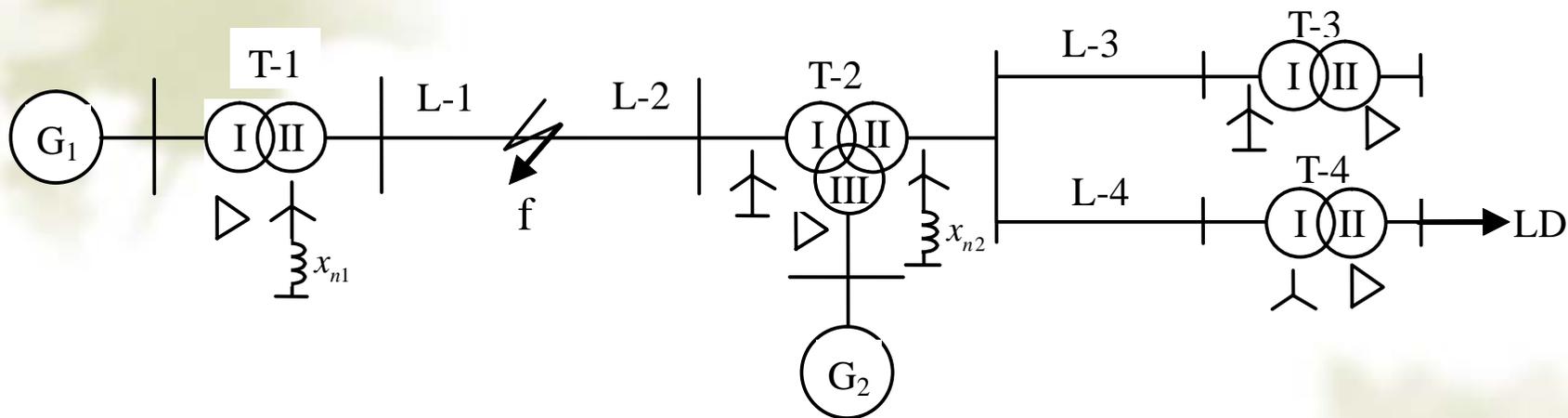
7-7 电力系统各序网络的制定

算例—正序网络



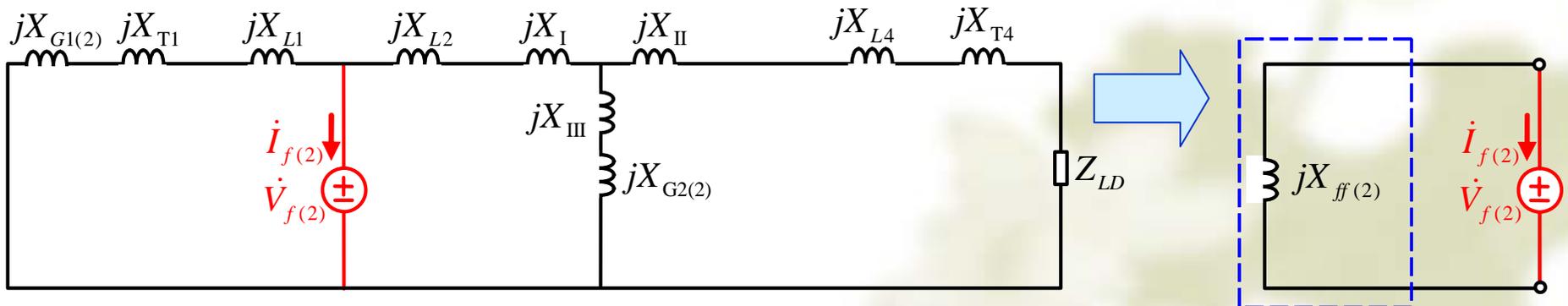
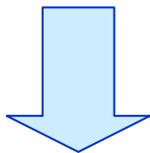
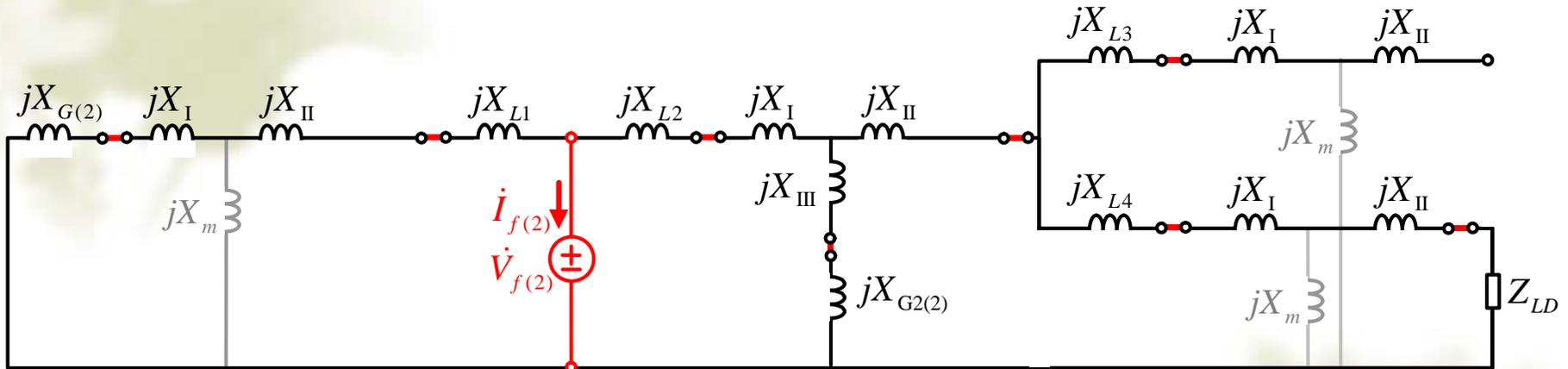
7-7 电力系统各序网络的制定

算例—负序网络



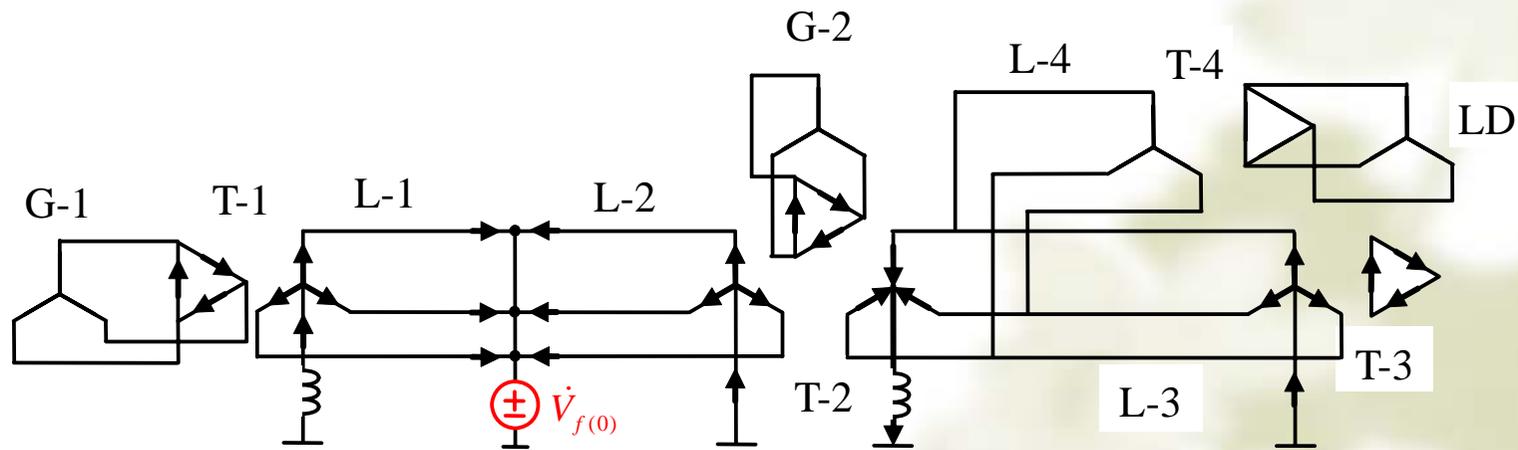
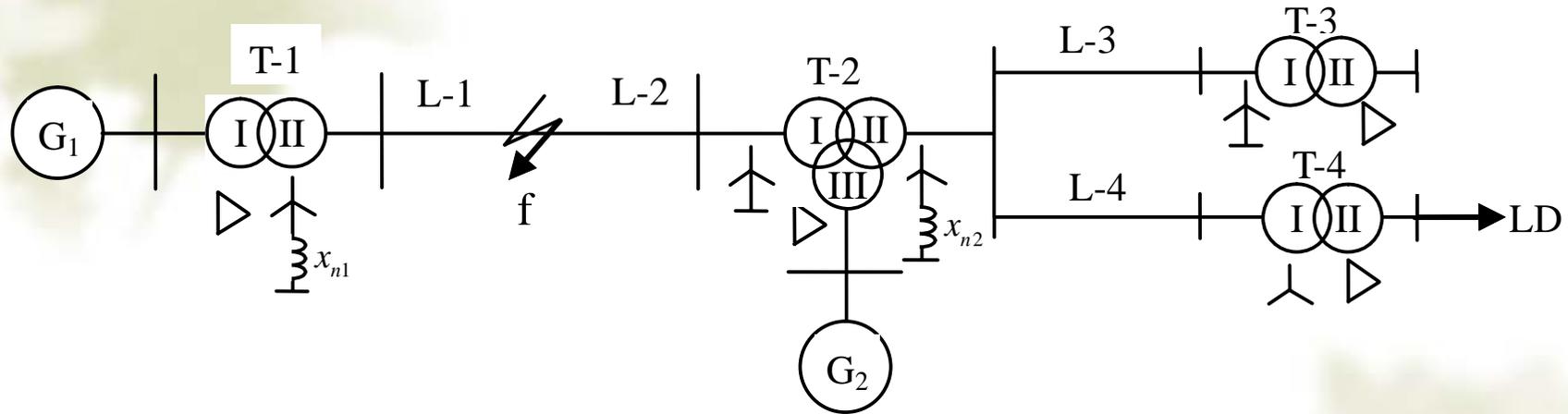
7-7 电力系统各序网络的制定

算例—负序网络



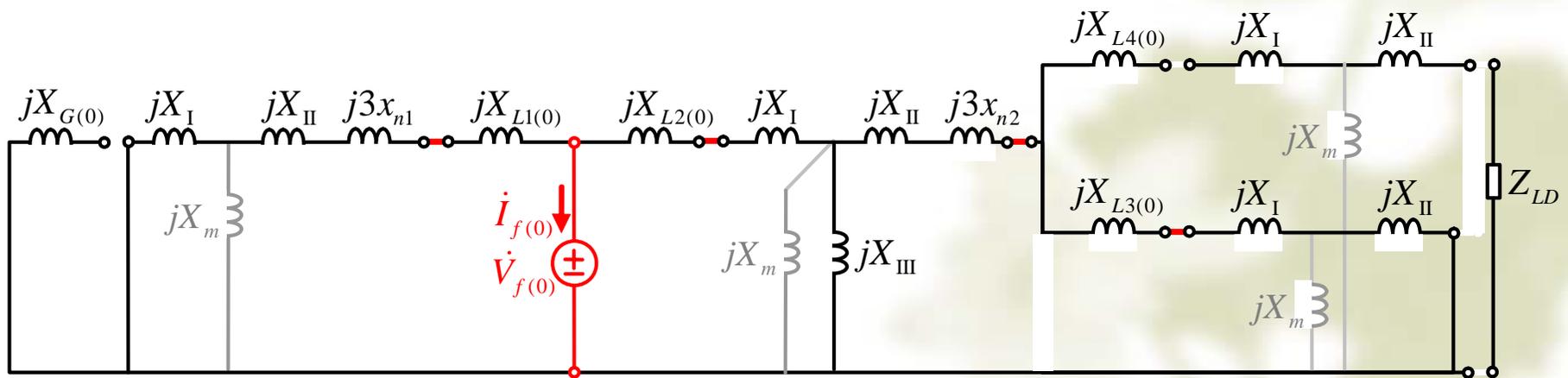
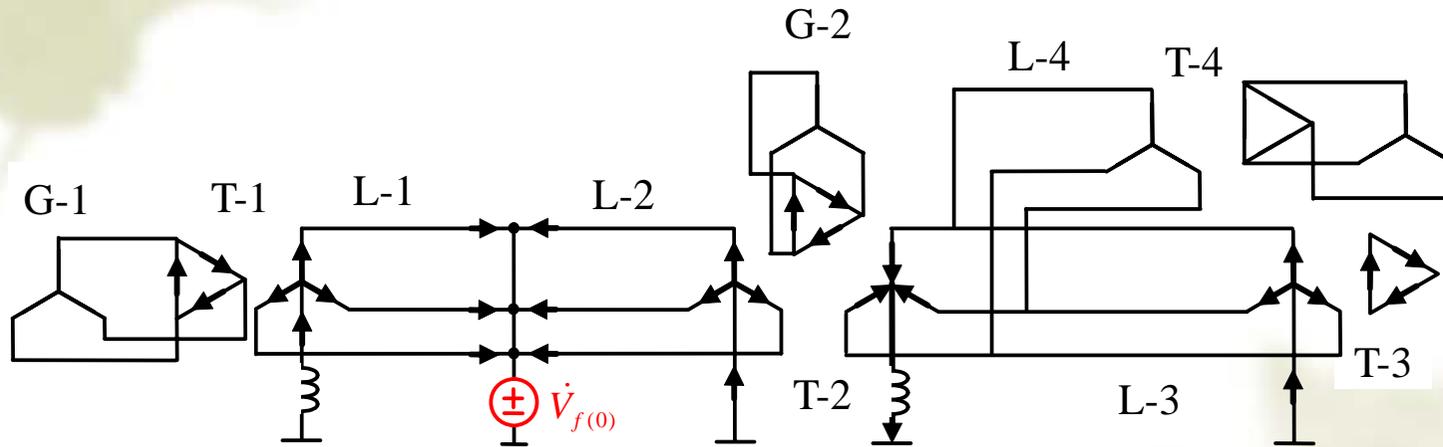
7-7 电力系统各序网络的制定

算例—零序网络



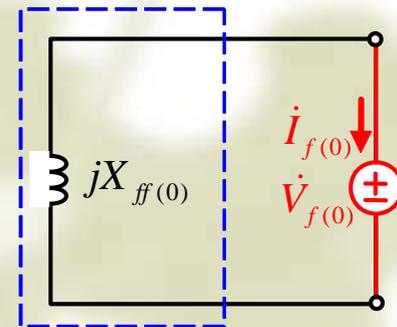
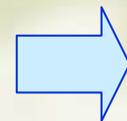
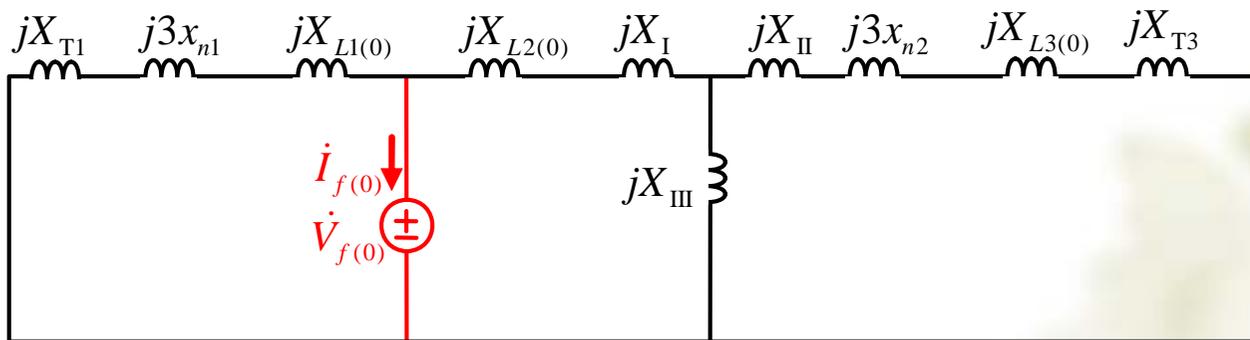
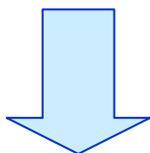
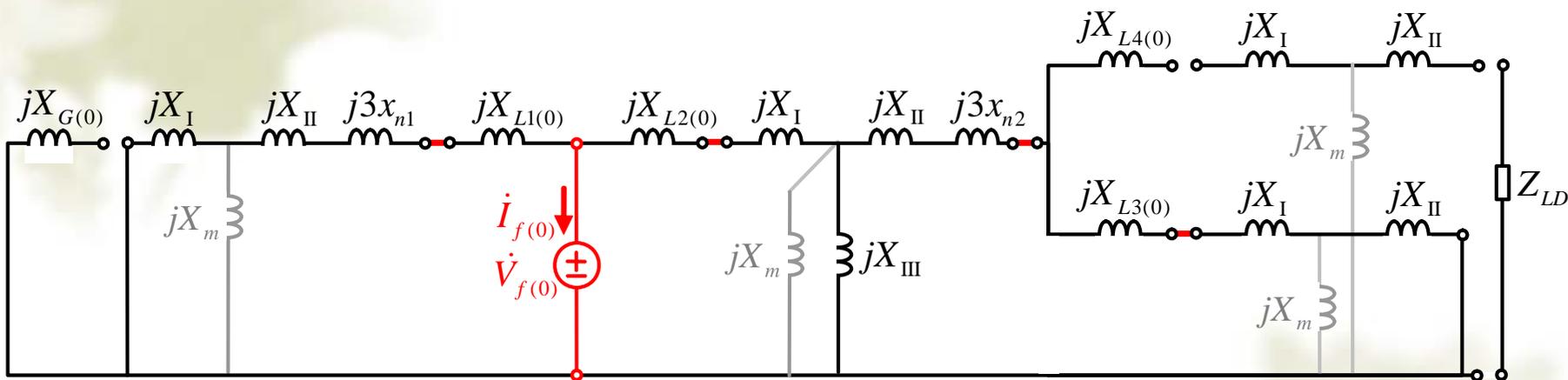
7-7 电力系统各序网络的制定

算例—零序网络



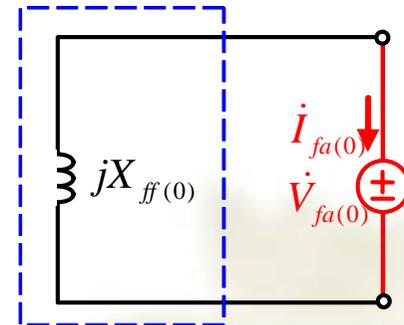
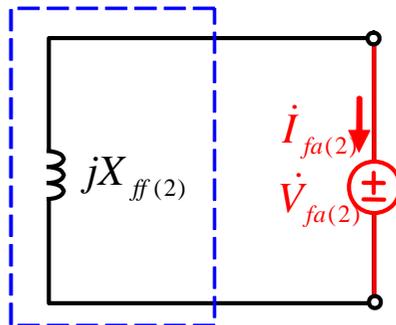
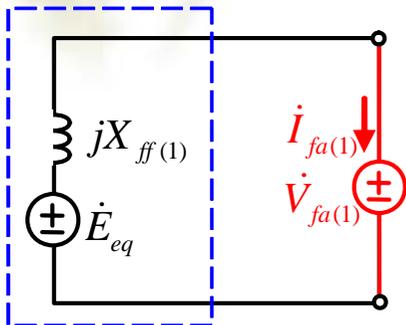
7-7 电力系统各序网络的制定

算例—零序网络



7-7 电力系统各序网络的制定

序网方程



$$\dot{V}_{fa(1)} = \dot{E}_{eq} - Z_{ff(1)} \dot{I}_{fa(1)}$$

$$\dot{V}_{fa(2)} = -Z_{ff(2)} \dot{I}_{fa(2)}$$

$$\dot{V}_{fa(0)} = -Z_{ff(0)} \dot{I}_{fa(0)}$$

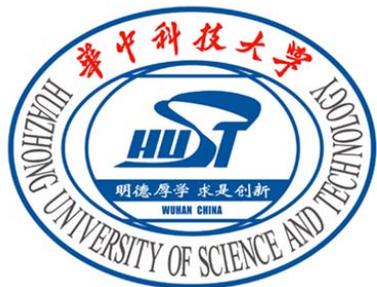


华中科技大学

Huazhong University of
Science and Technology

本章小结

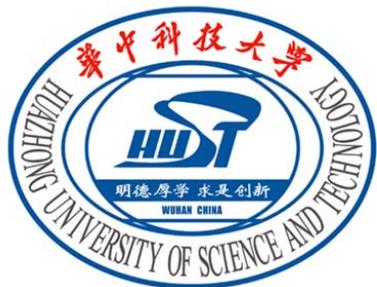
- ❖ 对称分量法分析不对称故障的原理和方法；
- ❖ 变压器的零序等值电路和参数；
- ❖ 输电线路零序等值电路及参数；
- ❖ 制定序网的原则和方法；



华中科技大学
Huazhong University of
Science and Technology

习 题

Ex 7-3, 7-5, 7-7



华中科技大学
Huazhong University of
Science and Technology



To Be Continued